

Progetto di riqualificazione per il cinema teatro Italia

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TITOLO ELABORATO

SCALA

RELAZIONE DI CALCOLO
STATO ATTUALE

-

CODICE ELABORATO

SD_002

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00	emissione	30.12.2021	-

TABULATI DI CALCOLO

(in ottemperanza al D.M. 17 genn. 2018 "Norme tecniche per le costruzioni" par. 10)

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CARATTERISTICHE MATERIALI UTILIZZATI

LEGENDA TABELLA DATI MATERIALI

Il programma consente l'uso di materiali diversi. Sono previsti i seguenti tipi di materiale:

1	materiale tipo cemento armato
2	materiale tipo acciaio
3	materiale tipo muratura
4	materiale tipo legno
5	materiale tipo generico

I materiali utilizzati nella modellazione sono individuati da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni materiale vengono riportati in tabella i seguenti dati:

Young	modulo di elasticità normale E
Poisson	coefficiente di contrazione trasversale ν
G	modulo di elasticità tangenziale
Gamma	peso specifico
Alfa	coefficiente di dilatazione termica
Fattore di confidenza FC m	Fattore di confidenza specifico per materiale; (è riportato solo se diverso da quello globale della struttura)
Fattore di confidenza FC a	Fattore di confidenza specifico per l'armatura (è riportato solo se diverso da quello globale della struttura)
Elasto-plastico	Materiale elastico perfettamente plastico per aste non lineari
Massima compressione	Massima tensione di compressione per aste non lineari
Massima trazione	Massima tensione di trazione per aste non lineari
Fattore attrito	Coefficiente di attrito per aste non lineari
Rapporto HRDb	Rapporto di hardening a flessione
Rapporto HRDv	Rapporto di hardening a taglio

I dati soprariportati vengono utilizzati per la modellazione dello schema statico e per la determinazione dei carichi inerziali e termici. In relazione al tipo di materiale vengono riportati inoltre:

1	c.a.	Resistenza Rc	resistenza a compressione cubica
		Resistenza fctm	resistenza media a trazione semplice
		Coefficiente ksb	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
2	acciaio	Tensione ft	Valore della tensione di rottura
		Tensione fy	Valore della tensione di snervamento
		Resistenza fd	Resistenza di calcolo per SL CNR-UNI 10011
		Resistenza fd (>40)	Resistenza di calcolo per SL CNR-UNI 10011 per spessori >

		40mm
	Tensione ammissibile	Tensione ammissibile CNR-UNI 10011
	Tensione ammissibile(>40)	Tensione ammissibile CNR-UNI 10011 per spessori > 40mm
3	muratura	
	Muratura consolidata	Muratura per la quale si prevedono interventi di rinforzo"
	Incremento resistenza	Incremento conseguito in termini di resistenza
	Incremento rigidezza	Incremento conseguito in termini di rigidezza
	Resistenza f	Valore della resistenza a compressione
	Resistenza fv0	Valore della resistenza a taglio in assenza di tensioni normali
	Resistenza fh	Valore della resistenza a compressione orizzontale
	Resistenza fb	Valore della resistenza a compressione dei blocchi
	Resistenza fbh	Valore della resistenza a compressione dei blocchi in direzione orizzontale
	Resistenza fv0h	Valore della resistenza a taglio in assenza di tensioni normali per le travi
	Resistenza ft	Valore della resistenza a trazione per fessurazione diagonale
	Resistenza fvlm	Valore della massima resistenza a taglio
	Resistenza fbt	Valore della resistenza a trazione dei blocchi
	Coefficiente mu	Coefficiente d'attrito utilizzato per la resistenza a taglio (tipicamente 0.4)
	Coefficiente fi	Coefficiente d'ingranamento utilizzato per la resistenza a taglio
	Coefficiente ksb	Coefficiente di riduzione della resistenza a compressione da utilizzare nello stress block
4	legno	
	E0,05	Modulo di elasticità corrispondente ad un frattile del 5%
	Resistenza fc0	Valore della resistenza a compressione parallela
	Resistenza ft0	Valore della resistenza a trazione parallela
	Resistenza fm	Valore della resistenza a flessione
	Resistenza fv	Valore della resistenza a taglio
	Resist. ft0k	Resistenza caratteristica (tensione amm. per REGLES) per trazione
	Resist. fmk	Resistenza caratteristica (tensione amm. per REGLES) per flessione
	Resist. fvk	Resistenza caratteristica (tensione amm. per REGLES) per taglio
	Modulo E0,05 Lamellare	Modulo elastico parallelo caratteristico lamellare o massiccio

Nel tabulato si riportano sia i valori caratteristici che medi utilizzando gli uni e/o gli altri in relazione alle richieste di normativa ed alla tipologia di verifica. (Cap.7 NTC18 per materiali nuovi, Cap.8 NTC18 e relativa circolare 21/01/2019 per materiali esistenti, Linee Guida Reluis per incamiciatura CAM, CNR-DT 200 per interventi con FRP)

Vengono inoltre riportate le tabelle contenenti il riassunto delle informazioni assegnate nei criteri di progetto in uso.

Id	Tipo / Note	V. caratt. daN/cm2	V. medio daN/cm2	Young daN/cm2	Poisson	G daN/cm2	Gamma daN/cm3	Alfa	Altri
11	Acciaio Fe360 - S235-acciaio Fe360-S235			2.100e+06	0.30	8.077e+05	7.85e-03	1.20e-05	
	Fattore di confidenza FC m								1.35
	Tensione ft	3420.0	3600.0						
	Tensione fy	2232.5	2350.0						
	Resistenza fd	2350.0							
	Resistenza fd (>40)	2100.0							
	Tensione ammissibile	1600.0							
	Tensione ammissibile (>40)	1400.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
12	Acciaio Fe430 - S275-acciaio Fe430-S275			2.100e+06	0.30	8.077e+05	7.85e-03	1.20e-05	
	Tensione ft	4300.0	4526.3						
	Tensione fy	2750.0	2894.7						
	Resistenza fd	2750.0							
	Resistenza fd (>40)	2500.0							
	Tensione ammissibile	1900.0							
	Tensione ammissibile (>40)	1700.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
108	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04			1.500e+04	0.0	5000.0	1.80e-03	1.00e-05	
	Fattore di confidenza FC m								1.35
	Resistenza f	20.8	34.5						
	Resistenza fh	10.4	20.0						
	Resistenza fv0	0.9	2.0						
	Resistenza fv0h	0.9	2.0						
	Resistenza tau0	0.3	0.9						
	Resistenza fvlm	2.4	3.4						
	Resistenza fb	41.6	52.0						
	Resistenza fbh	8.3	10.4						
	Resistenza fbt	2.2	2.8						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Coefficiente mu tilda								0.50
	Coefficiente fi								0.50
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
158	Calcestruzzo Classe C25/30			3.145e+05	0.20	1.310e+05	2.50e-03	1.00e-05	
	Fattore di confidenza FC m								1.35
	Fattore di confidenza FC a								1.35
	Resistenza Rc	203.6	300.0						
	Resistenza fctm		25.6						
	Rapporto Rfessurata								1.00
	Coefficiente ksb								0.85
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05
159	Acciaio Fe430 - S275-acciaio Fe430-S275			2.100e+06	0.30	8.077e+05	7.85e-03	1.20e-05	
	Fattore di confidenza FC m								1.35
	Tensione ft	4085.0	4300.0						
	Tensione fy	2612.5	2750.0						
	Resistenza fd	2750.0							
	Resistenza fd (>40)	2500.0							
	Tensione ammissibile	1900.0							
	Tensione ammissibile (>40)	1700.0							
	Rapporto HRDb								1.00e-05
	Rapporto HRDv								1.00e-05

Aste acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Beta assegnato	0.80	0.80	0.80	0.80	0.80	
Verifica come controvento	NO	NO	NO	NO	NO	
Usa condizioni I e II	SI	SI	SI	SI	SI	
Coefficiente gamma M0	1.05	1.05	1.05	1.05	1.05	
Coefficiente gamma M1	1.05	1.05	1.05	1.05	1.05	
Coefficiente gamma M2	1.25	1.25	1.25	1.25	1.25	

Travi acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
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INGEGNERE

Travi acc.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
3-3 Beta * L automatico	SI	SI	SI	SI	SI	
3-3 Beta assegnato	1.00	1.00	1.00	1.00	1.00	
3-3 Beta assegnato [cm]	0.0	0.0	0.0	0.0	0.0	
2-2 Beta * L automatico	SI	SI	SI	SI	SI	
2-2 Beta assegnato	1.00	1.00	1.00	1.00	1.00	
2-2 Beta * L assegnato [cm]	0.0	0.0	0.0	0.0	0.0	
1-1 Beta * L automatico	SI	SI	SI	SI	SI	
1-1 Beta assegnato	1.00	1.00	1.00	1.00	1.00	
1-1 Beta * L assegnato [cm]	0.0	0.0	0.0	0.0	0.0	
Generalità						
Coefficiente gamma M0	1.05	1.05	1.05	1.05	1.05	
Coefficiente gamma M1	1.05	1.05	1.05	1.05	1.05	
Coefficiente gamma M2	1.25	1.25	1.25	1.25	1.25	
Luce di taglio per GR [cm]	1.00	1.00	1.00	1.00	1.00	
Usa condizioni I e II	SI	SI	SI	SI	SI	
Momenti equivalenti	SI	SI	SI	SI	SI	

Gusci c.a.	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Armatura						
Inclinazione Ax [gradi]	0.0	0.0	0.0	0.0	0.0	
Angolo Ax-Ay [gradi]	90.00	90.00	90.00	90.00	90.00	
Minima tesa	0.31	0.10	0.13	2.000e-02	0.31	
Massima tesa	0.78	4.00	4.00	4.00	0.78	
Maglia unica centrale	NO	NO	NO	NO	NO	
Copriferro [cm]	2.00	3.00	2.00	2.00	2.00	
Maglia x						
diametro	10	12	10	10	10	
passo	20	20	20	20	20	
diametro aggiuntivi	12	12	12	12	12	
Maglia y						
diametro	10	12	10	10	10	
passo	20	20	20	20	20	
diametro aggiuntivi	12	12	12	12	12	
Stati limite ultimi						
Tensione fy [daN/cm2]	4500.00	4500.00	4500.00	4500.00	4500.00	
Tipo acciaio	tipo C	tipo C	tipo C	tipo C	tipo C	
Coefficiente gamma s	1.15	1.15	1.15	1.15	1.15	
Coefficiente gamma c	1.50	1.50	1.50	1.50	1.50	
Verifiche con N costante	SI	SI	SI	SI	SI	
Applica SLU da DIN	NO	NO	NO	NO	NO	
Tensioni ammissibili						
Tensione amm. cls [daN/cm2]	97.50	97.50	97.50	97.50	97.50	
Tensione amm. acciaio [daN/cm2]	2600.00	2600.00	2600.00	2600.00	2600.00	
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00	15.00	
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00	1.00	
Resistenza al fuoco						
3- intradosso	NO	NO	NO	NO	NO	
3+ estradosso	NO	NO	NO	NO	NO	
Tempo di esposizione R	15	15	15	15	15	

Muratura	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Lunghezze libere						
Altezza interpiano [cm]	0.0	0.0	0.0	0.0	0.0	
Rho	0.85	0.85	0.85	0.85	0.85	
Snellezza limite	20.00	20.00	20.00	20.00	20.00	
Generalità						
Gamma non sismico	3.00	3.00	3.00	3.00	3.00	
Gamma sismico	2.40	2.40	2.40	2.00	2.40	
Tolleranza azioni [daN/cm2]	0.0	0.0	0.0	0.0	0.0	
Media valori per quota	SI	SI	SI	SI	SI	
Media valori per elemento	SI	SI	SI	SI	SI	
Verifica come fascia	NO	NO	NO	NO	SI	
Usa formula [7.8.3]	SI	SI	SI	SI	SI	

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Generalità						
Usa tensioni ammissibili	NO	NO	NO	NO	NO	
Af inf: da traliccio	SI	SI	SI	SI	SI	
Consenti armatura a taglio	NO	NO	NO	NO	NO	

INGEGNERE

Solai e pannelli	1/7/..	2/8/..	3/9/..	4/10/..	5/11/..	6/12/..
Incrementa armatura longitudinale per taglio	SI	SI	SI	SI	SI	
Af inf: da $q \cdot L \cdot L /$	20.00	20.00	20.00	20.00	20.00	
Incremento fascia piena [cm]	5.00	5.00	5.00	5.00	5.00	
Armatura						
Minima tesa	0.15	0.15	0.15	0.15	0.15	
Massima tesa	3.00	3.00	3.00	3.00	3.00	
Minima compressa	0.0	0.0	0.0	0.0	0.0	
Af/h [cm]	7.000e-02	7.000e-02	7.000e-02	7.000e-02	7.000e-02	
Stati limite ultimi						
Tensione f_y [daN/cm ²]	4500.00	4500.00	4500.00	4500.00	4500.00	
Tipo acciaio	tipo C	tipo C	tipo C	tipo C	tipo C	
Coefficiente gamma s	1.15	1.15	1.15	1.15	1.15	
Coefficiente gamma c	1.50	1.50	1.50	1.50	1.50	
Fattore di ridistribuzione	0.0	0.0	0.0	0.0	0.0	
Tensioni ammissibili						
Tensione amm. cls [daN/cm ²]	85.00	85.00	85.00	85.00	85.00	
Tensione amm. acciaio [daN/cm ²]	2600.00	2600.00	2600.00	2600.00	2600.00	
Rapporto omogeneizzazione N	15.00	15.00	15.00	15.00	15.00	
Massimo rapporto area compressa/tesa	1.00	1.00	1.00	1.00	1.00	
Verifica freccia						
Infinita	250.00	250.00	250.00	250.00	250.00	
Istantanea	500.00	500.00	500.00	500.00	500.00	
Fattore viscosità	3.00	3.00	3.00	3.00	3.00	
Usa J non fessurato	NO	NO	NO	NO	NO	
Elementi non strutturali						
Tamponatura antiespulsione	NO	NO	NO	NO	NO	
Tamponatura con armatura	NO	NO	NO	NO	NO	
Fattore di struttura/comportamento	2.00	2.00	2.00	2.00	2.00	
Coefficiente gamma m	0.0	0.0	0.0	0.0	0.0	
Periodo Ta	0.0	0.0	0.0	0.0	0.0	
Altezza pannello	0.0	0.0	0.0	0.0	0.0	

MODELLAZIONE DELLE SEZIONI

LEGENDA TABELLA DATI SEZIONI

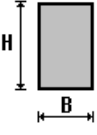
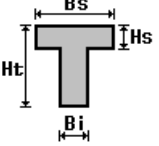
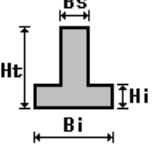
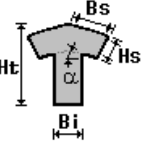
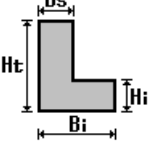
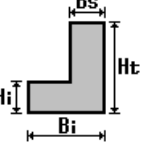
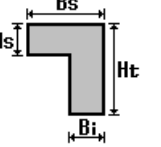
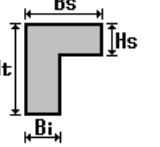
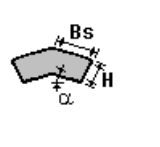
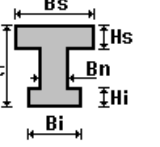
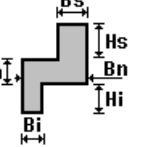
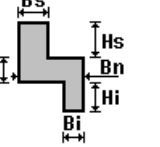
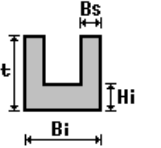
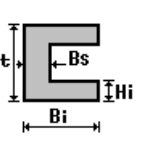
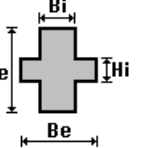
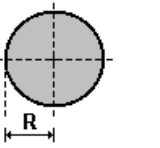
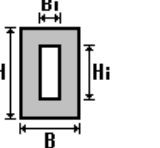
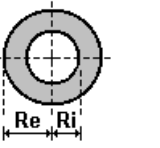
Il programma consente l'uso di sezioni diverse. Sono previsti i seguenti tipi di sezione:

1. sezione di tipo generico
2. profilati semplici
3. profilati accoppiati e speciali

Le sezioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni sezione vengono riportati in tabella i seguenti dati:

Area	area della sezione
A V2	area della sezione/fattore di taglio (per il taglio in direzione 2)
A V3	area della sezione/fattore di taglio (per il taglio in direzione 3)
Jt	fattore torsionale di rigidezza
J2-2	momento d'inerzia della sezione riferito all'asse 2
J3-3	momento d'inerzia della sezione riferito all'asse 3
W2-2	modulo di resistenza della sezione riferito all'asse 2
W3-3	modulo di resistenza della sezione riferito all'asse 3
Wp2-2	modulo di resistenza plastico della sezione riferito all'asse 2
Wp3-3	modulo di resistenza plastico della sezione riferito all'asse 3

I dati sopra riportati vengono utilizzati per la determinazione dei carichi inerziali e per la definizione delle rigidezze degli elementi strutturali; qualora il valore di Area V2 (e/o Area V3) sia nullo la deformabilità per taglio V2 (e/o V3) è trascurata. La valutazione delle caratteristiche inerziali delle sezioni è condotta nel riferimento 2-3 dell'elemento.

 rettangolare	 a T	 a T rovescia	 a T di colmo	 a L	 a L specchiata
 a L specchiata rovescia	 a L rovescia	 a L di colmo	 a doppio T	 a quattro specchiata	 a quattro
 a U	 a C	 a croce	 circolare	 rettangolare cava	 circolare cava

Per quanto concerne i profilati semplici ed accoppiati l'asse 2 del riferimento coincide con l'asse x riportato nei più diffusi profilati.

Per quanto concerne le sezioni di tipo generico (tipo 1.):
 i valori dimensionali con prefisso B sono riferiti all'asse 2
 i valori dimensionali con prefisso H sono riferiti all'asse 3

Id	Tipo	Area	A V2	A V3	Jt	J 2-2	J 3-3	W 2-2	W 3-3	Wp 2-2	Wp 3-3
		cm2	cm2	cm2	cm4	cm4	cm4	cm3	cm3	cm3	cm3
1	Rettangolare: b=51 h=51	2601.00	2167.50	2167.50	9.510e+05	5.638e+05	5.638e+05	2.211e+04	2.211e+04	3.316e+04	3.316e+04
2	Rettangolare: b=38 h=38	1444.00	1203.33	1203.33	2.931e+05	1.738e+05	1.738e+05	9145.33	9145.33	1.372e+04	1.372e+04
3	IPE 140	16.40	0.0	0.0	2.40	45.00	541.00	12.30	77.30	19.20	88.30
4	T.QU 40x3	4.44	0.0	0.0	15.20	10.19	10.19	5.09	5.09	6.17	6.17
5	Rettangolare: b=25 h=25	625.00	520.83	520.83	5.491e+04	3.255e+04	3.255e+04	2604.17	2604.17	3906.25	3906.25
6	IPE 200	28.50	0.0	0.0	7.00	142.00	1943.00	28.50	194.30	44.60	220.60
7	IPN 180	27.80	0.0	0.0	9.60	81.30	1450.00	19.80	161.00	33.20	187.00
8	HEA 200	53.80	0.0	0.0	21.00	1336.00	3692.00	133.60	388.60	203.80	429.50

MODELLAZIONE STRUTTURA: NODI

LEGENDA TABELLA DATI NODI

Il programma utilizza per la modellazione nodi strutturali.

Ogni nodo è individuato dalle coordinate cartesiane nel sistema di riferimento globale (X Y Z).

Ad ogni nodo è eventualmente associato un codice di vincolamento rigido, un codice di fondazione speciale, ed un set di sei molle (tre per le traslazioni, tre per le rotazioni). Le tabelle sottoriportate riflettono le succitate possibilità. In particolare per ogni nodo viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z

Per i nodi ai quali sia associato un codice di vincolamento rigido, un codice di fondazione speciale o un set di molle viene indicato in tabella:

Nodo	numero del nodo.
X	valore della coordinata X
Y	valore della coordinata Y
Z	valore della coordinata Z
Note	eventuale codice di vincolo (es. v=110010 sei valori relativi ai sei gradi di libertà previsti per il nodo TxTyTzRxRyRz, il valore 1 indica che lo spostamento o rotazione relativo è impedito, il valore 0 indica che lo spostamento o rotazione relativo è libero).
Note	(FS = 1, 2,...) eventuale codice del tipo di fondazione speciale (1, 2,... fanno riferimento alle tipologie: plinto, palo, plinto su pali,...) che è collegato al nodo. (ISO = "id SIGLA") indice e sigla identificativa dell' eventuale isolatore sismico assegnato al nodo
Rig. TX	valore della rigidezza dei vincoli elastici eventualmente applicati al nodo, nello specifico TX (idem per TY, TZ, RX, RY, RZ).

Per strutture sismicamente isolate viene inoltre inserita la tabella delle caratteristiche per gli isolatori utilizzati; le caratteristiche sono indicate in conformità al cap. 7.10 del D.M. 17/01/18

TABELLA DATI NODI

Nodo	X	Y	Z	Nodo	X	Y	Z	Nodo	X	Y	Z
	cm	cm	cm		cm	cm	cm		cm	cm	cm
2	6.0	1055.3	106.7	3	108.4	1055.3	106.7	5	6.0	1055.3	220.0
6	108.4	1055.3	220.0	7	6.0	1055.3	320.0	8	108.4	1055.3	320.0
9	210.8	1055.3	106.7	11	210.8	1055.3	220.0	12	210.8	1055.3	320.0
13	313.2	1055.3	106.7	15	313.2	1055.3	220.0	16	313.2	1055.3	320.0
17	415.6	1055.3	106.7	19	415.6	1055.3	220.0	20	415.6	1055.3	320.0
21	506.5	1055.3	106.7	23	506.5	1055.3	220.0	24	506.5	1055.3	320.0
25	597.3	1055.3	106.7	27	597.3	1055.3	220.0	28	597.3	1055.3	320.0
29	688.2	1055.3	106.7	31	688.2	1055.3	220.0	32	688.2	1055.3	320.0
33	779.0	1055.3	106.7	35	779.0	1055.3	220.0	36	779.0	1055.3	320.0
37	860.9	1055.3	106.7	39	860.9	1055.3	220.0	40	860.9	1055.3	320.0
41	985.1	1055.3	106.7	43	985.1	1055.3	220.0	44	985.1	1055.3	320.0
45	1064.5	1055.3	106.7	47	1064.5	1055.3	220.0	48	1064.5	1055.3	320.0
49	1143.8	1055.3	106.7	51	1143.8	1055.3	220.0	52	1143.8	1055.3	320.0
53	1228.2	1055.3	106.7	55	1228.2	1055.3	220.0	56	1228.2	1055.3	320.0
57	1312.5	1055.3	106.7	59	1312.5	1055.3	220.0	60	1312.5	1055.3	320.0

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61	1434.5	1055.3	106.7	63	1434.5	1055.3	220.0	64	1434.5	1055.3	320.0
65	1508.7	1055.3	106.7	67	1508.7	1055.3	220.0	68	1508.7	1055.3	320.0
69	1611.1	1055.3	106.7	71	1611.1	1055.3	220.0	72	1611.1	1055.3	320.0
73	1713.5	1055.3	106.7	75	1713.5	1055.3	220.0	76	1713.5	1055.3	320.0
77	1793.5	1055.3	106.7	79	1793.5	1055.3	220.0	80	1793.5	1055.3	320.0
81	1873.5	1055.3	106.7	83	1873.5	1055.3	220.0	84	1873.5	1055.3	320.0
85	1925.6	1055.3	106.7	87	1925.6	1055.3	220.0	88	1925.6	1055.3	320.0
90	2117.3	1055.3	106.7	91	2197.0	1055.3	106.7	93	2117.3	1055.3	220.0
94	2197.0	1055.3	220.0	95	2117.3	1055.3	320.0	96	2197.0	1055.3	320.0
97	2276.7	1055.3	106.7	99	2276.7	1055.3	220.0	100	2276.7	1055.3	320.0
101	2021.5	1055.3	220.0	102	2021.5	1055.3	320.0	104	6.0	-1.4	106.7
105	108.4	-1.4	106.7	107	6.0	-1.4	220.0	108	108.4	-1.4	220.0
109	6.0	-1.4	320.0	110	108.4	-1.4	320.0	111	210.8	-1.4	106.7
113	210.8	-1.4	220.0	114	210.8	-1.4	320.0	115	313.2	-1.4	106.7
117	313.2	-1.4	220.0	118	313.2	-1.4	320.0	119	415.6	-1.4	106.7
121	415.6	-1.4	220.0	122	415.6	-1.4	320.0	123	506.5	-1.4	106.7
125	506.5	-1.4	220.0	126	506.5	-1.4	320.0	127	597.3	-1.4	106.7
129	597.3	-1.4	220.0	130	597.3	-1.4	320.0	131	688.2	-1.4	106.7
133	688.2	-1.4	220.0	134	688.2	-1.4	320.0	135	779.0	-1.4	106.7
137	779.0	-1.4	220.0	138	779.0	-1.4	320.0	139	870.2	-1.4	106.7
141	870.2	-1.4	220.0	142	870.2	-1.4	320.0	143	961.4	-1.4	106.7
145	961.4	-1.4	220.0	146	961.4	-1.4	320.0	147	1052.6	-1.4	106.7
149	1052.6	-1.4	220.0	150	1052.6	-1.4	320.0	151	1143.8	-1.4	106.7
153	1143.8	-1.4	220.0	154	1143.8	-1.4	320.0	155	1235.0	-1.4	106.7
157	1235.0	-1.4	220.0	158	1235.0	-1.4	320.0	159	1326.2	-1.4	106.7
161	1326.2	-1.4	220.0	162	1326.2	-1.4	320.0	163	1417.4	-1.4	106.7
165	1417.4	-1.4	220.0	166	1417.4	-1.4	320.0	167	1508.7	-1.4	106.7
169	1508.7	-1.4	220.0	170	1508.7	-1.4	320.0	171	1611.1	-1.4	106.7
173	1611.1	-1.4	220.0	174	1611.1	-1.4	320.0	175	1713.5	-1.4	106.7
177	1713.5	-1.4	220.0	178	1713.5	-1.4	320.0	179	1793.5	-1.4	106.7
181	1793.5	-1.4	220.0	182	1793.5	-1.4	320.0	183	1873.5	-1.4	106.7
185	1873.5	-1.4	220.0	186	1873.5	-1.4	320.0	187	1974.3	-1.4	106.7
189	1974.3	-1.4	220.0	190	1974.3	-1.4	320.0	191	2075.1	-1.4	106.7
193	2075.1	-1.4	220.0	194	2075.1	-1.4	320.0	195	2175.9	-1.4	106.7
197	2175.9	-1.4	220.0	198	2175.9	-1.4	320.0	199	2276.7	-1.4	106.7
201	2276.7	-1.4	220.0	202	2276.7	-1.4	320.0	203	2276.7	115.8	106.7
205	2276.7	115.8	220.0	206	2276.7	115.8	320.0	207	2276.7	250.9	106.7
209	2276.7	250.9	220.0	210	2276.7	250.9	320.0	211	2276.7	349.4	106.7
213	2276.7	349.4	220.0	214	2276.7	349.4	320.0	215	2276.7	458.2	106.7
217	2276.7	458.2	220.0	218	2276.7	458.2	320.0	219	2276.7	593.2	106.7
221	2276.7	593.2	220.0	222	2276.7	593.2	320.0	223	2276.6	701.6	106.7
225	2276.6	701.6	220.0	226	2276.7	701.6	320.0	227	2276.7	805.6	106.7
229	2276.7	805.6	220.0	230	2276.7	805.6	320.0	231	2276.7	940.6	106.7
233	2276.7	940.6	220.0	234	2276.7	940.6	320.0	235	2276.7	1215.0	106.7
237	2276.7	1215.0	220.0	238	2276.7	1215.0	320.0	239	2276.7	1347.9	106.7
241	2276.7	1347.9	220.0	242	2276.7	1347.9	320.0	243	2276.7	1523.5	106.7
245	2276.7	1523.5	220.0	246	2276.7	1523.5	320.0	247	6.0	965.0	533.9
248	6.0	965.0	620.0	249	6.0	1120.5	106.7	251	2276.7	593.2	920.0
252	6.0	1120.5	220.0	253	1713.5	-147.0	426.7	254	6.0	1120.5	320.0
255	6.0	1185.7	106.7	257	6.0	1185.7	220.0	258	6.0	1185.7	320.0
259	6.0	1282.8	106.7	261	6.0	1282.8	220.0	262	6.0	1282.8	320.0
263	100.6	1292.9	106.7	265	100.6	1292.9	220.0	266	100.6	1292.9	320.0
267	195.2	1302.9	106.7	269	195.2	1302.9	220.0	270	195.2	1302.9	320.0
271	289.8	1312.9	106.7	273	289.8	1312.9	220.0	274	289.8	1312.9	320.0
275	384.5	1322.9	106.7	277	384.5	1322.9	220.0	278	384.5	1322.9	320.0
279	479.1	1333.0	106.7	281	479.1	1333.0	220.0	282	479.1	1333.0	320.0
283	573.7	1343.0	106.7	285	573.7	1343.0	220.0	286	573.7	1343.0	320.0
287	668.3	1353.0	106.7	289	668.3	1353.0	220.0	290	668.3	1353.0	320.0
291	762.9	1363.1	106.7	293	762.9	1363.1	220.0	294	762.9	1363.1	320.0
295	857.5	1373.1	106.7	297	857.5	1373.1	220.0	298	857.5	1373.1	320.0
299	952.1	1383.1	106.7	301	952.1	1383.1	220.0	302	952.1	1383.1	320.0
303	1046.7	1393.2	106.7	305	1046.7	1393.2	220.0	306	1046.7	1393.2	320.0
307	1141.4	1403.2	106.7	309	1141.4	1403.2	220.0	310	1141.4	1403.2	320.0
311	1236.0	1413.2	106.7	313	1236.0	1413.2	220.0	314	1236.0	1413.2	320.0
315	1330.6	1423.2	106.7	317	1330.6	1423.2	220.0	318	1330.6	1423.2	320.0
319	1425.2	1433.3	106.7	321	1425.2	1433.3	220.0	322	1425.2	1433.3	320.0
323	1519.8	1443.3	106.7	325	1519.8	1443.3	220.0	326	1519.8	1443.3	320.0
327	1614.4	1453.3	106.7	329	1614.4	1453.3	220.0	330	1614.4	1453.3	320.0
331	1709.0	1463.4	106.7	333	1709.0	1463.4	220.0	334	1709.0	1463.4	320.0
335	1803.6	1473.4	106.7	337	1803.6	1473.4	220.0	338	1803.6	1473.4	320.0
339	1898.3	1483.4	106.7	341	1898.3	1483.4	220.0	342	1898.3	1483.4	320.0
343	1992.9	1493.4	106.7	345	1992.9	1493.4	220.0	346	1992.9	1493.4	320.0
347	2087.5	1503.5	106.7	349	2087.5	1503.5	220.0	350	2087.5	1503.5	320.0
351	2182.1	1513.5	106.7	353	2182.1	1513.5	220.0	354	2182.1	1513.5	320.0
356	2276.7	1373.3	106.7	357	2276.7	1373.3	220.0	358	2276.7	1373.3	320.0
360	1799.2	1339.8	106.7	361	1894.7	1346.5	106.7	363	1799.2	1339.8	220.0
364	1894.7	1346.5	220.0	365	1799.2	1339.8	320.0	366	1894.7	1346.5	320.0
367	1990.2	1353.2	106.7	369	1990.2	1353.2	220.0	370	1990.2	1353.2	320.0
371	2085.7	1359.9	106.7	373	2085.7	1359.9	220.0	374	2085.7	1359.9	320.0

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375	2181.2	1366.6	106.7	377	2181.2	1366.6	220.0	378	2181.2	1366.6	320.0
379	1785.8	1471.5	106.7	381	1785.8	1471.5	220.0	382	1785.8	1471.5	320.0
383	6.0	75.9	106.7	385	6.0	75.9	220.0	386	6.0	75.9	320.0
387	6.0	153.3	106.7	389	6.0	153.3	220.0	390	6.0	153.3	320.0
391	6.0	280.4	106.7	393	6.0	280.4	220.0	394	6.0	280.4	320.0
395	6.0	403.7	106.7	397	6.0	403.7	220.0	398	6.0	403.7	320.0
399	6.0	526.1	106.7	401	6.0	526.1	220.0	402	6.0	526.1	320.0
403	6.0	607.8	106.7	405	6.0	607.8	220.0	406	6.0	607.8	320.0
407	5.9	701.6	106.7	409	5.9	701.6	220.0	410	6.0	701.6	320.0
411	6.0	771.3	106.7	413	6.0	771.3	220.0	414	6.0	771.3	320.0
415	6.0	874.6	106.7	417	6.0	874.6	220.0	418	6.0	874.6	320.0
419	6.0	965.0	106.7	421	6.0	965.0	220.0	422	6.0	965.0	320.0
423	-88.9	153.3	106.7	425	-88.9	153.3	220.0	426	-88.9	153.3	320.0
427	-183.9	153.3	106.7	429	-183.9	153.3	220.0	430	-183.9	153.3	320.0
431	-235.5	153.3	106.7	433	-235.5	153.3	220.0	434	-235.5	153.3	320.0
435	-327.5	153.3	106.7	437	-327.5	153.3	220.0	438	-327.5	153.3	320.0
439	-378.4	153.3	106.7	441	-378.4	153.3	220.0	442	-378.4	153.3	320.0
443	-447.2	153.3	106.7	445	-447.2	153.3	220.0	446	-447.2	153.3	320.0
447	-516.0	153.3	106.7	449	-516.0	153.3	220.0	450	-516.0	153.3	320.0
451	-584.7	153.3	106.7	453	-584.7	153.3	220.0	454	-584.7	153.3	320.0
455	-584.7	246.5	106.7	457	-584.7	246.5	220.0	458	-584.7	246.5	320.0
459	-584.7	339.7	106.7	461	-584.7	339.7	220.0	462	-584.7	339.7	320.0
463	-584.7	432.9	106.7	465	-584.7	432.9	220.0	466	-584.7	432.9	320.0
467	-584.7	526.1	106.7	469	-584.7	526.1	220.0	470	-584.7	526.1	320.0
471	-584.7	592.1	106.7	473	-584.7	592.1	220.0	474	-584.7	592.1	320.0
475	-584.7	658.2	106.7	477	-584.7	658.2	220.0	478	-584.7	658.2	320.0
479	-584.7	794.0	106.7	481	-584.7	794.0	220.0	482	-584.7	794.0	320.0
483	-584.7	874.6	106.7	485	-584.7	874.6	220.0	486	-584.7	874.6	320.0
487	-516.0	874.6	106.7	489	-516.0	874.6	220.0	490	-516.0	874.6	320.0
491	-447.2	874.6	106.7	493	-447.2	874.6	220.0	494	-447.2	874.6	320.0
495	-378.4	874.6	106.7	497	-378.4	874.6	220.0	498	-378.4	874.6	320.0
499	-313.6	874.6	106.7	501	-313.6	874.6	220.0	502	-313.6	874.6	320.0
503	-248.7	874.6	106.7	505	-248.7	874.6	220.0	506	-248.7	874.6	320.0
507	-183.9	874.6	106.7	509	-183.9	874.6	220.0	510	-183.9	874.6	320.0
511	-88.9	874.6	106.7	513	-88.9	874.6	220.0	514	-88.9	874.6	320.0
516	1903.5	701.6	320.0	518	1903.5	349.4	320.0	520	6.0	349.4	320.0
521	2276.7	701.6	726.7	522	1807.3	-147.0	620.0	523	6.0	349.4	106.7
524	6.0	349.4	220.0	525	2276.7	-147.0	106.7	527	2276.7	701.6	820.0
528	2276.7	-147.0	220.0	529	2276.7	-147.0	320.0	530	2182.8	-147.0	106.7
532	2182.8	-147.0	220.0	533	2182.8	-147.0	320.0	534	2089.0	-147.0	106.7
536	2089.0	-147.0	220.0	537	2089.0	-147.0	320.0	538	1995.1	-147.0	106.7
540	1995.1	-147.0	220.0	541	1995.1	-147.0	320.0	542	1901.2	-147.0	106.7
544	1901.2	-147.0	220.0	545	1901.2	-147.0	320.0	546	1807.3	-147.0	106.7
548	1807.3	-147.0	220.0	549	1807.3	-147.0	320.0	550	1713.5	-147.0	106.7
552	1713.5	-147.0	220.0	553	1713.5	-147.0	320.0	554	6.0	607.8	726.7
555	2276.7	701.6	920.0	556	6.0	1055.3	426.7	557	108.4	1055.3	426.7
558	2276.7	805.6	726.7	559	6.0	1055.3	533.9	560	108.4	1055.3	533.9
561	6.0	1055.3	620.0	562	108.4	1055.3	620.0	563	210.8	1055.3	426.7
564	1713.5	-147.0	533.9	565	210.8	1055.3	533.9	566	210.8	1055.3	620.0
567	313.2	1055.3	426.7	568	1713.5	-147.0	620.0	569	313.2	1055.3	533.9
570	313.2	1055.3	620.0	571	415.6	1055.3	426.7	572	2276.7	805.6	820.0
573	415.6	1055.3	533.9	574	415.6	1055.3	620.0	575	506.5	1055.3	426.7
576	-88.9	153.3	409.5	577	506.5	1055.3	533.9	578	506.5	1055.3	620.0
579	597.3	1055.3	426.7	580	-183.9	153.3	392.4	581	597.3	1055.3	533.9
582	597.3	1055.3	620.0	583	688.2	1055.3	426.7	584	2276.7	1055.3	820.0
585	688.2	1055.3	533.9	586	688.2	1055.3	620.0	587	779.0	1055.3	426.7
588	-235.5	153.3	383.1	589	779.0	1055.3	533.9	590	779.0	1055.3	620.0
591	860.9	1055.3	426.7	592	-327.5	153.3	366.4	593	860.9	1055.3	533.9
594	860.9	1055.3	620.0	595	985.1	1055.3	426.7	596	-378.4	153.3	357.3
597	985.1	1055.3	533.9	598	985.1	1055.3	620.0	599	1064.5	1055.3	426.7
600	779.0	527.0	620.0	601	1064.5	1055.3	533.9	602	1064.5	1055.3	620.0
603	1143.8	1055.3	426.7	604	-447.2	153.3	344.8	605	1143.8	1055.3	533.9
606	1143.8	1055.3	620.0	607	1228.2	1055.3	426.7	608	-516.0	153.3	332.4
609	1228.2	1055.3	533.9	610	1228.2	1055.3	620.0	611	1312.5	1055.3	426.7
612	2276.7	593.2	726.7	613	1312.5	1055.3	533.9	614	1312.5	1055.3	620.0
615	1434.5	1055.3	426.7	616	779.0	527.0	820.0	617	1434.5	1055.3	533.9
618	1434.5	1055.3	620.0	619	1508.7	1055.3	426.7	620	779.0	791.1	620.0
621	1508.7	1055.3	533.9	622	1508.7	1055.3	620.0	623	1611.1	1055.3	426.7
624	2276.7	593.2	820.0	625	1611.1	1055.3	533.9	626	1611.1	1055.3	620.0
627	1713.5	1055.3	426.7	628	2276.7	1055.3	920.0	629	1713.5	1055.3	533.9
630	1713.5	1055.3	620.0	631	1793.5	1055.3	426.7	632	779.0	262.8	620.0
633	1793.5	1055.3	533.9	634	1793.5	1055.3	620.0	635	1873.5	1055.3	426.7
636	779.0	350.8	753.3	637	1873.5	1055.3	533.9	638	1873.5	1055.3	620.0
639	1925.6	1055.3	426.7	640	6.0	1185.7	570.6	641	1925.6	1055.3	533.9
642	1925.6	1055.3	620.0	643	6.0	608.4	789.2	644	2117.3	1055.3	426.7
645	2197.0	1055.3	426.7	646	779.0	174.7	686.7	647	2117.3	1055.3	533.9
648	2197.0	1055.3	533.9	649	2117.3	1055.3	620.0	650	2197.0	1055.3	620.0
651	2276.7	1055.3	426.7	652	6.0	874.6	688.4	653	2276.7	1055.3	533.9
654	2276.7	1055.3	620.0	655	2021.5	1055.3	533.9	656	2021.5	1055.3	620.0

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657	2276.7	-1.4	726.7	658	6.0	-1.4	426.7	659	108.4	-1.4	426.7
660	779.0	703.1	753.3	661	6.0	-1.4	533.9	662	108.4	-1.4	533.9
663	6.0	-1.4	620.0	664	108.4	-1.4	620.0	665	210.8	-1.4	426.7
666	779.0	879.2	686.7	667	210.8	-1.4	533.9	668	210.8	-1.4	620.0
669	313.2	-1.4	426.7	670	2276.7	-1.4	820.0	671	313.2	-1.4	533.9
672	313.2	-1.4	620.0	673	415.6	-1.4	426.7	674	2276.7	-1.4	920.0
675	415.6	-1.4	533.9	676	415.6	-1.4	620.0	677	506.5	-1.4	426.7
678	2276.7	115.8	726.7	679	506.5	-1.4	533.9	680	506.5	-1.4	620.0
681	597.3	-1.4	426.7	682	415.6	527.0	620.0	683	597.3	-1.4	533.9
684	597.3	-1.4	620.0	685	688.2	-1.4	426.7	686	415.6	527.0	820.0
687	688.2	-1.4	533.9	688	688.2	-1.4	620.0	689	779.0	-1.4	426.7
690	2276.7	115.8	820.0	691	779.0	-1.4	533.9	692	779.0	-1.4	620.0
693	870.2	-1.4	426.7	694	2276.7	115.8	920.0	695	870.2	-1.4	533.9
696	870.2	-1.4	620.0	697	961.4	-1.4	426.7	698	415.6	791.1	620.0
699	961.4	-1.4	533.9	700	961.4	-1.4	620.0	701	1052.6	-1.4	426.7
702	2276.7	250.9	726.7	703	1052.6	-1.4	533.9	704	1052.6	-1.4	620.0
705	1143.8	-1.4	426.7	706	415.6	262.8	620.0	707	1143.8	-1.4	533.9
708	1143.8	-1.4	620.0	709	1235.0	-1.4	426.7	710	2276.7	250.9	820.0
711	1235.0	-1.4	533.9	712	1235.0	-1.4	620.0	713	1326.2	-1.4	426.7
714	415.6	350.8	753.3	715	1326.2	-1.4	533.9	716	1326.2	-1.4	620.0
717	1417.4	-1.4	426.7	718	2276.7	250.9	920.0	719	1417.4	-1.4	533.9
720	1417.4	-1.4	620.0	721	1508.7	-1.4	426.7	722	2276.7	349.4	726.7
723	1508.7	-1.4	533.9	724	1508.7	-1.4	620.0	725	1611.1	-1.4	426.7
726	415.6	174.7	686.7	727	1611.1	-1.4	533.9	728	1611.1	-1.4	620.0
729	1713.5	-1.4	426.7	730	415.6	703.1	753.3	731	1713.5	-1.4	533.9
732	1713.5	-1.4	620.0	733	1793.5	-1.4	426.7	734	2276.7	349.4	820.0
735	1793.5	-1.4	533.9	736	1793.5	-1.4	620.0	737	1873.5	-1.4	426.7
738	2276.7	349.4	920.0	739	1873.5	-1.4	533.9	740	1873.5	-1.4	620.0
741	1974.3	-1.4	426.7	742	2276.7	458.2	726.7	743	1974.3	-1.4	533.9
744	1974.3	-1.4	620.0	745	2075.1	-1.4	426.7	746	415.6	879.2	686.7
747	2075.1	-1.4	533.9	748	2075.1	-1.4	620.0	749	2175.9	-1.4	426.7
750	1143.8	527.0	620.0	751	2175.9	-1.4	533.9	752	2175.9	-1.4	620.0
753	2276.7	-1.4	426.7	754	2276.7	458.2	820.0	755	2276.7	-1.4	533.9
756	2276.7	-1.4	620.0	757	2276.7	115.8	426.7	758	2276.7	458.2	920.0
759	2276.7	115.8	533.9	760	2276.7	115.8	620.0	761	2276.7	250.9	426.7
762	1143.8	527.0	820.0	763	2276.7	250.9	533.9	764	2276.7	250.9	620.0
765	2276.7	349.4	426.7	766	2276.7	805.6	920.0	767	2276.7	349.4	533.9
768	2276.7	349.4	620.0	769	2276.7	458.2	426.7	770	2276.7	940.6	726.7
771	2276.7	458.2	533.9	772	2276.7	458.2	620.0	773	2276.7	593.2	426.7
774	1143.8	791.1	620.0	775	2276.7	593.2	533.9	776	2276.7	593.2	620.0
777	2276.7	701.6	426.7	778	6.0	965.0	426.7	779	2276.7	701.6	533.9
780	2276.7	701.6	620.0	781	2276.7	805.6	426.7	782	1143.8	262.8	620.0
783	2276.7	805.6	533.9	784	2276.7	805.6	620.0	785	2276.7	940.6	426.7
786	2276.7	940.6	820.0	787	2276.7	940.6	533.9	788	2276.7	940.6	620.0
789	2276.7	1215.0	426.7	790	2276.7	940.6	920.0	791	2276.7	1215.0	533.9
792	2276.7	1215.0	620.0	793	2276.7	1347.9	426.7	794	6.0	349.4	726.7
795	2276.7	1347.9	533.9	796	2276.7	1347.9	620.0	797	2276.7	1523.5	426.7
798	1143.8	350.8	753.3	799	2276.7	1523.5	533.9	800	2276.7	1523.5	620.0
801	1143.8	174.7	686.7	802	2276.7	458.2	794.0	803	6.0	1120.5	426.7
804	2276.7	593.2	794.9	805	1143.8	703.1	753.3	806	6.0	1120.5	533.9
807	1143.8	879.2	686.7	808	6.0	527.0	820.0	809	6.0	1185.7	426.7
810	1508.7	527.0	620.0	811	6.0	1185.7	533.9	812	2276.7	527.0	726.7
813	6.0	1282.8	426.7	814	2276.7	805.6	714.5	815	6.0	1282.8	533.9
816	6.0	153.3	620.0	817	100.6	1292.9	426.7	818	1508.7	527.0	820.0
819	100.6	1292.9	533.9	820	2276.7	773.5	726.7	821	195.2	1302.9	426.7
822	1508.7	791.1	620.0	823	195.2	1302.9	533.9	824	1508.7	262.8	620.0
825	289.8	1312.9	426.7	826	1508.7	350.8	753.3	827	289.8	1312.9	533.9
828	6.0	280.4	726.7	829	384.5	1322.9	426.7	830	2276.7	940.6	663.4
831	384.5	1322.9	533.9	832	6.0	280.4	620.0	833	479.1	1333.0	426.7
834	2276.7	701.6	753.9	835	479.1	1333.0	533.9	836	1508.7	174.7	686.7
837	573.7	1343.0	426.7	838	1508.7	703.1	753.3	839	573.7	1343.0	533.9
840	6.0	404.1	773.5	841	668.3	1353.0	426.7	842	2021.5	1055.3	426.7
843	668.3	1353.0	533.9	844	6.0	403.7	726.7	845	762.9	1363.1	426.7
846	-516.0	874.6	332.4	847	762.9	1363.1	533.9	848	6.0	403.7	620.0
849	857.5	1373.1	426.7	850	-447.2	874.6	344.8	851	857.5	1373.1	533.9
852	6.0	349.4	752.8	853	952.1	1383.1	426.7	854	1508.7	879.2	686.7
855	952.1	1383.1	533.9	856	6.0	75.9	649.3	857	1046.7	1393.2	426.7
858	-378.4	874.6	357.3	859	1046.7	1393.2	533.9	860	2276.7	250.9	715.5
861	1141.4	1403.2	426.7	862	-313.6	874.6	369.0	863	1141.4	1403.2	533.9
864	6.0	773.5	726.7	865	1236.0	1413.2	426.7	866	-248.7	874.6	380.7
867	1236.0	1413.2	533.9	868	6.0	75.9	620.0	869	1330.6	1423.2	426.7
870	1873.5	527.0	620.0	871	1330.6	1423.2	533.9	872	6.0	701.6	726.7
873	1425.2	1433.3	426.7	874	-183.9	874.6	392.4	875	1425.2	1433.3	533.9
876	6.0	965.0	654.2	877	1519.8	1443.3	426.7	878	-88.9	874.6	409.5
879	1519.8	1443.3	533.9	880	1873.5	527.0	820.0	881	1614.4	1453.3	426.7
882	-378.4	525.3	357.3	883	1614.4	1453.3	533.9	884	1873.5	791.1	620.0
885	1709.0	1463.4	426.7	886	-183.9	525.3	392.4	887	1709.0	1463.4	533.9
888	2276.7	280.4	726.7	889	1803.6	1473.4	426.7	890	1873.5	262.8	620.0
891	1803.6	1473.4	533.9	892	2276.7	527.0	920.0	893	1898.3	1483.4	426.7

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894	1873.5	350.8	753.3	895	1898.3	1483.4	533.9	896	1873.5	174.7	686.7
897	1992.9	1493.4	426.7	898	1873.5	703.1	753.3	899	1992.9	1493.4	533.9
900	1992.9	1493.4	555.4	901	2087.5	1503.5	426.7	902	6.0	349.4	426.7
903	2087.5	1503.5	533.9	904	2087.5	1503.5	576.9	905	2182.1	1513.5	426.7
906	6.0	349.4	533.9	907	2182.1	1513.5	533.9	908	2182.1	1513.5	598.5
909	2276.7	-147.0	426.7	910	2276.7	1373.3	426.7	911	2276.7	1373.3	533.9
912	2276.7	1373.3	620.0	913	1873.5	879.2	686.7	914	6.0	526.1	726.0
915	6.0	1120.5	595.3	916	2276.7	-147.0	533.9	917	6.0	349.4	620.0
918	6.0	771.3	620.0	919	2276.7	-147.0	620.0	920	6.0	526.1	620.0
921	2276.7	527.0	620.0	922	2276.7	527.0	220.0	923	6.0	153.3	678.6
924	2182.8	-147.0	426.7	925	2276.7	527.0	820.0	926	1582.4	855.0	320.0
927	2276.7	527.0	320.0	928	2276.7	527.0	426.7	929	2276.7	527.0	533.9
930	2182.8	-147.0	533.9	931	2276.7	349.4	752.8	932	2276.7	115.8	664.4
933	1785.8	1471.5	426.7	934	2182.8	-147.0	620.0	935	1785.8	1471.5	533.9
936	6.0	701.6	753.9	937	6.0	75.9	426.7	938	2089.0	-147.0	426.7
939	6.0	75.9	533.9	940	1713.5	855.0	320.0	941	6.0	153.3	426.7
942	2089.0	-147.0	533.9	943	6.0	153.3	533.9	944	2089.0	-147.0	620.0
945	6.0	280.4	426.7	946	1995.1	-147.0	426.7	947	6.0	280.4	533.9
948	1591.6	212.0	320.0	949	6.0	403.7	426.7	950	1995.1	-147.0	533.9
951	6.0	403.7	533.9	952	1995.1	-147.0	620.0	953	6.0	526.1	426.7
954	1901.2	-147.0	426.7	955	6.0	526.1	533.9	956	2276.7	1055.3	726.7
957	6.0	607.8	426.7	958	1901.2	-147.0	533.9	959	6.0	607.8	533.9
960	6.0	607.8	620.0	961	6.0	701.6	426.7	962	1901.2	-147.0	620.0
963	6.0	701.6	533.9	964	6.0	701.6	620.0	965	6.0	771.3	426.7
966	1807.3	-147.0	426.7	967	6.0	771.3	533.9	968	1713.5	211.2	320.0
969	6.0	874.6	426.7	970	1807.3	-147.0	533.9	971	6.0	874.6	533.9
972	6.0	874.6	620.0	973	2376.2	1534.1	320.0	974	2376.7	-147.0	320.0

Nodo	X	Y	Z	Note	Rig. TX	Rig. TY	Rig. TZ	Rig. RX	Rig. RY	Rig. RZ
	cm	cm	cm		daN/cm	daN/cm	daN/cm	daN cm/rad	daN cm/rad	daN cm/rad
1	6.0	1055.3	0.0	v=111111						
4	108.4	1055.3	0.0	v=111111						
10	210.8	1055.3	0.0	v=111111						
14	313.2	1055.3	0.0	v=111111						
18	415.6	1055.3	0.0	v=111111						
22	506.5	1055.3	0.0	v=111111						
26	597.3	1055.3	0.0	v=111111						
30	688.2	1055.3	0.0	v=111111						
34	779.0	1055.3	0.0	v=111111						
38	860.9	1055.3	0.0	v=111111						
42	985.1	1055.3	0.0	v=111111						
46	1064.5	1055.3	0.0	v=111111						
50	1143.8	1055.3	0.0	v=111111						
54	1228.2	1055.3	0.0	v=111111						
58	1312.5	1055.3	0.0	v=111111						
62	1434.5	1055.3	0.0	v=111111						
66	1508.7	1055.3	0.0	v=111111						
70	1611.1	1055.3	0.0	v=111111						
74	1713.5	1055.3	0.0	v=111111						
78	1793.5	1055.3	0.0	v=111111						
82	1873.5	1055.3	0.0	v=111111						
86	1925.6	1055.3	0.0	v=111111						
89	2117.3	1055.3	0.0	v=111111						
92	2197.0	1055.3	0.0	v=111111						
98	2276.7	1055.3	0.0	v=111111						
103	6.0	-1.4	0.0	v=111111						
106	108.4	-1.4	0.0	v=111111						
112	210.8	-1.4	0.0	v=111111						
116	313.2	-1.4	0.0	v=111111						
120	415.6	-1.4	0.0	v=111111						
124	506.5	-1.4	0.0	v=111111						
128	597.3	-1.4	0.0	v=111111						
132	688.2	-1.4	0.0	v=111111						
136	779.0	-1.4	0.0	v=111111						
140	870.2	-1.4	0.0	v=111111						
144	961.4	-1.4	0.0	v=111111						
148	1052.6	-1.4	0.0	v=111111						
152	1143.8	-1.4	0.0	v=111111						
156	1235.0	-1.4	0.0	v=111111						
160	1326.2	-1.4	0.0	v=111111						
164	1417.4	-1.4	0.0	v=111111						
168	1508.7	-1.4	0.0	v=111111						
172	1611.1	-1.4	0.0	v=111111						
176	1713.5	-1.4	0.0	v=111111						
180	1793.5	-1.4	0.0	v=111111						
184	1873.5	-1.4	0.0	v=111111						
188	1974.3	-1.4	0.0	v=111111						
192	2075.1	-1.4	0.0	v=111111						

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196	2175.9	-1.4	0.0	v=111111
200	2276.7	-1.4	0.0	v=111111
204	2276.7	115.8	0.0	v=111111
208	2276.7	250.9	0.0	v=111111
212	2276.7	349.4	0.0	v=111111
216	2276.7	458.2	0.0	v=111111
220	2276.7	593.2	0.0	v=111111
224	2276.6	701.6	0.0	v=111111
228	2276.7	805.6	0.0	v=111111
232	2276.7	940.6	0.0	v=111111
236	2276.7	1215.0	0.0	v=111111
240	2276.7	1347.9	0.0	v=111111
244	2276.7	1523.5	0.0	v=111111
250	6.0	1120.5	0.0	v=111111
256	6.0	1185.7	0.0	v=111111
260	6.0	1282.8	0.0	v=111111
264	100.6	1292.9	0.0	v=111111
268	195.2	1302.9	0.0	v=111111
272	289.8	1312.9	0.0	v=111111
276	384.5	1322.9	0.0	v=111111
280	479.1	1333.0	0.0	v=111111
284	573.7	1343.0	0.0	v=111111
288	668.3	1353.0	0.0	v=111111
292	762.9	1363.1	0.0	v=111111
296	857.5	1373.1	0.0	v=111111
300	952.1	1383.1	0.0	v=111111
304	1046.7	1393.2	0.0	v=111111
308	1141.4	1403.2	0.0	v=111111
312	1236.0	1413.2	0.0	v=111111
316	1330.6	1423.2	0.0	v=111111
320	1425.2	1433.3	0.0	v=111111
324	1519.8	1443.3	0.0	v=111111
328	1614.4	1453.3	0.0	v=111111
332	1709.0	1463.4	0.0	v=111111
336	1803.6	1473.4	0.0	v=111111
340	1898.3	1483.4	0.0	v=111111
344	1992.9	1493.4	0.0	v=111111
348	2087.5	1503.5	0.0	v=111111
352	2182.1	1513.5	0.0	v=111111
355	2276.7	1373.3	0.0	v=111111
359	1799.2	1339.8	0.0	v=111111
362	1894.7	1346.5	0.0	v=111111
368	1990.2	1353.2	0.0	v=111111
372	2085.7	1359.9	0.0	v=111111
376	2181.2	1366.6	0.0	v=111111
380	1785.8	1471.5	0.0	v=111111
384	6.0	75.9	0.0	v=111111
388	6.0	153.3	0.0	v=111111
392	6.0	280.4	0.0	v=111111
396	6.0	403.7	0.0	v=111111
400	6.0	526.1	0.0	v=111111
404	6.0	607.8	0.0	v=111111
408	5.9	701.6	0.0	v=111111
412	6.0	771.3	0.0	v=111111
416	6.0	874.6	0.0	v=111111
420	6.0	965.0	0.0	v=111111
424	-88.9	153.3	0.0	v=111111
428	-183.9	153.3	0.0	v=111111
432	-235.5	153.3	0.0	v=111111
436	-327.5	153.3	0.0	v=111111
440	-378.4	153.3	0.0	v=111111
444	-447.2	153.3	0.0	v=111111
448	-516.0	153.3	0.0	v=111111
452	-584.7	153.3	0.0	v=111111
456	-584.7	246.5	0.0	v=111111
460	-584.7	339.7	0.0	v=111111
464	-584.7	432.9	0.0	v=111111
468	-584.7	526.1	0.0	v=111111
472	-584.7	592.1	0.0	v=111111
476	-584.7	658.2	0.0	v=111111
480	-584.7	794.0	0.0	v=111111
484	-584.7	874.6	0.0	v=111111
488	-516.0	874.6	0.0	v=111111
492	-447.2	874.6	0.0	v=111111
496	-378.4	874.6	0.0	v=111111
500	-313.6	874.6	0.0	v=111111
504	-248.7	874.6	0.0	v=111111
508	-183.9	874.6	0.0	v=111111
512	-88.9	874.6	0.0	v=111111

INGEGNERE

515	1903.5	701.6	0.0	v=111111
517	1903.5	349.4	0.0	v=111111
519	6.0	349.4	0.0	v=111111
526	2276.7	-147.0	0.0	v=111111
531	2182.8	-147.0	0.0	v=111111
535	2089.0	-147.0	0.0	v=111111
539	1995.1	-147.0	0.0	v=111111
543	1901.2	-147.0	0.0	v=111111
547	1807.3	-147.0	0.0	v=111111
551	1713.5	-147.0	0.0	v=111111

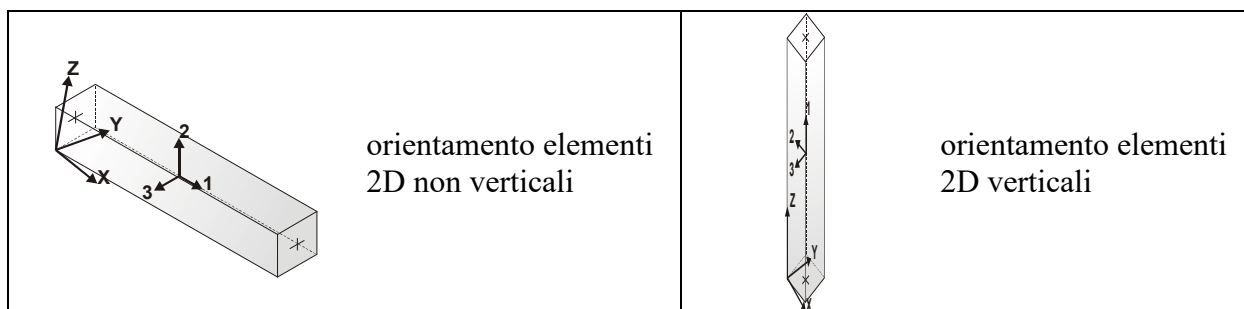
MODELLAZIONE STRUTTURA: ELEMENTI TRAVE

TABELLA DATI TRAVI

Il programma utilizza per la modellazione elementi a due nodi denominati in generale travi.

Ogni elemento trave è individuato dal nodo iniziale e dal nodo finale.

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione.



In particolare per ogni elemento viene indicato in tabella:

Elem.	numero dell'elemento
Note	codice di comportamento: trave, trave di fondazione, pilastro, asta, asta tesa, asta compressa,
Nodo I (J)	numero del nodo iniziale (finale)
Mat.	codice del materiale assegnato all'elemento
Sez.	codice della sezione assegnata all'elemento
Rotaz.	valore della rotazione dell'elemento, attorno al proprio asse, nel caso in cui l'orientamento di default non sia adottabile; l'orientamento di default prevede per gli elementi non verticali l'asse 2 contenuto nel piano verticale e l'asse 3 orizzontale, per gli elementi verticali l'asse 2 diretto secondo X negativo e l'asse 3 diretto secondo Y negativo
Svincolo I (J)	codici di svincolo per le azioni interne; i primi sei codici si riferiscono al nodo iniziale, i restanti sei al nodo finale (il valore 1 indica che la relativa azione interna non è attiva)
Wink V	costante di sottofondo (coefficiente di Winkler) per la modellazione della trave su suolo elastico
Wink O	costante di sottofondo (coefficiente di Winkler) per la modellazione del suolo elastico orizzontale

Elem.	Note	Nodo I	Nodo J	Mat.	Sez.	Crit.	Rotaz. gradi	Svincolo I	Svincolo J	Wink V daN/cm3	Wink O daN/cm3
1	Asta	646	632	11	4	1					
2	Asta	632	636	11	4	1					
3	Asta	636	600	11	4	1					
4	Asta	600	660	11	4	1					
5	Asta	660	620	11	4	1					
6	Asta	620	666	11	4	1					
7	Asta	600	616	11	4	1					
8	Asta	726	706	11	4	1					
9	Asta	706	714	11	4	1					
10	Asta	714	682	11	4	1					
11	Asta	682	730	11	4	1					
12	Asta	730	698	11	4	1					
13	Asta	698	746	11	4	1					
14	Asta	682	686	11	4	1					
15	Asta	801	782	11	4	1					
16	Asta	782	798	11	4	1					
17	Asta	798	750	11	4	1					
18	Asta	750	805	11	4	1					
19	Asta	805	774	11	4	1					
20	Asta	774	807	11	4	1					
21	Asta	750	762	11	4	1					
22	Asta	836	824	11	4	1					
23	Asta	824	826	11	4	1					
24	Asta	826	810	11	4	1					
25	Asta	810	838	11	4	1					
26	Asta	838	822	11	4	1					
27	Asta	822	854	11	4	1					
28	Asta	810	818	11	4	1					
29	Asta	896	890	11	4	1					
30	Asta	890	894	11	4	1					
31	Asta	894	870	11	4	1					
32	Asta	870	898	11	4	1					
33	Asta	898	884	11	4	1					
34	Asta	884	913	11	4	1					
35	Asta	870	880	11	4	1					
36	Pilas.	109	658	108	1	1					
37	Pilas.	410	961	108	1	1					
38	Pilas.	520	902	108	1	1					
39	Trave	692	646	159	3	1		000001			
40	Trave	616	660	159	3	1					
41	Trave	692	632	159	3	1		000001			
42	Pilas.	515	516	108	2	1					
43	Pilas.	517	518	108	2	1					
44	Pilas.	18	17	108	1	1					
45	Pilas.	34	33	108	1	1					
46	Pilas.	50	49	108	1	1					
47	Pilas.	66	65	108	1	1					
48	Pilas.	82	81	108	1	1					
49	Trave	636	616	159	3	1					
50	Trave	660	666	159	3	1					
51	Trave	600	620	159	3	1					
52	Trave	646	636	159	3	1					
53	Trave	632	600	159	3	1					
54	Trave	666	590	159	3	1				000001	
55	Trave	620	590	159	3	1				000001	
56	Trave	676	726	159	3	1		000001			
57	Trave	686	730	159	3	1					
58	Trave	676	706	159	3	1		000001			
59	Pilas.	98	97	108	1	1					
60	Pilas.	224	223	108	1	1					
61	Pilas.	212	211	108	1	1					
62	Pilas.	200	199	108	1	1					
63	Pilas.	184	183	108	1	1					
64	Pilas.	168	167	108	1	1					
65	Pilas.	152	151	108	1	1					
66	Trave	714	686	159	3	1					
67	Trave	730	746	159	3	1					
68	Trave	682	698	159	3	1					
69	Trave	726	714	159	3	1					
70	Trave	706	682	159	3	1					
71	Trave	746	574	159	3	1				000001	
72	Trave	698	574	159	3	1				000001	
73	Trave	708	801	159	3	1		000001			
74	Trave	762	805	159	3	1					

INGEGNERE

75	Trave	708	782	159	3	1	000001	
76	Pilas.	136	135	108	1	1		
77	Pilas.	120	119	108	1	1		
78	Pilas.	103	104	108	1	1		
79	Pilas.	408	407	108	1	1		
80	Pilas.	519	523	108	1	1		
81	Trave	886	874	159	3	1		
82	Trave	882	858	159	3	1		
83	Trave	798	762	159	3	1		
84	Trave	805	807	159	3	1		
85	Trave	750	774	159	3	1		
86	Trave	801	798	159	3	1		
87	Trave	782	750	159	3	1		
88	Trave	807	606	159	3	1		000001
89	Trave	774	606	159	3	1		000001
90	Trave	724	836	159	3	1	000001	
91	Trave	818	838	159	3	1		
92	Trave	724	824	159	3	1	000001	
93	Pilas.	20	571	108	1	1		
94	Pilas.	36	587	108	1	1		
95	Pilas.	52	603	108	1	1		
96	Pilas.	68	619	108	1	1		
97	Pilas.	84	635	108	1	1		
98	Pilas.	100	651	108	1	1		
99	Pilas.	226	777	108	1	1		
100	Trave	826	818	159	3	1		
101	Trave	838	854	159	3	1		
102	Trave	810	822	159	3	1		
103	Trave	836	826	159	3	1		
104	Trave	824	810	159	3	1		
105	Trave	854	622	159	3	1		000001
106	Trave	822	622	159	3	1		000001
107	Trave	740	896	159	3	1	000001	
108	Trave	880	898	159	3	1		
109	Trave	740	890	159	3	1	000001	
110	Pilas.	214	765	108	1	1		
111	Pilas.	202	753	108	1	1		
112	Pilas.	186	737	108	1	1		
113	Pilas.	170	721	108	1	1		
114	Pilas.	154	705	108	1	1		
115	Pilas.	138	689	108	1	1		
116	Pilas.	122	673	108	1	1		
117	Trave	894	880	159	3	1		
118	Trave	898	913	159	3	1		
119	Trave	870	884	159	3	1		
120	Trave	896	894	159	3	1		
121	Trave	890	870	159	3	1		
122	Trave	913	638	159	3	1		000001
123	Trave	884	638	159	3	1		000001
124	Pilas.	654	956	108	1	1		
125	Pilas.	780	521	108	1	1		
126	Pilas.	768	722	108	1	1		
127	Pilas.	756	657	108	1	1		
128	Pilas.	917	794	108	1	1		
129	Pilas.	964	872	108	1	1		
130	Pilas.	658	661	108	1	1		
131	Pilas.	961	963	108	1	1		
132	Pilas.	902	906	108	1	1		
133	Pilas.	794	852	108	1	1		
134	Pilas.	872	936	108	1	1		
135	Pilas.	661	663	108	1	1		
136	Pilas.	963	964	108	1	1		
137	Pilas.	906	917	108	1	1		
138	Pilas.	931	734	108	1	1		
139	Pilas.	571	573	108	1	1		
140	Pilas.	587	589	108	1	1		
141	Pilas.	603	605	108	1	1		
142	Pilas.	619	621	108	1	1		
143	Pilas.	635	637	108	1	1		
144	Pilas.	651	653	108	1	1		
145	Pilas.	777	779	108	1	1		
146	Pilas.	765	767	108	1	1		
147	Pilas.	753	755	108	1	1		
148	Pilas.	737	739	108	1	1		
149	Pilas.	721	723	108	1	1		
150	Pilas.	705	707	108	1	1		
151	Pilas.	689	691	108	1	1		
152	Pilas.	673	675	108	1	1		
153	Pilas.	956	584	108	1	1		

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154	Pilas.	521	834	108	1	1		
155	Pilas.	722	931	108	1	1		
156	Pilas.	657	670	108	1	1		
157	Pilas.	734	738	108	1	1		
158	Pilas.	573	574	108	1	1		
159	Pilas.	589	590	108	1	1		
160	Pilas.	605	606	108	1	1		
161	Pilas.	621	622	108	1	1		
162	Pilas.	637	638	108	1	1		
163	Pilas.	653	654	108	1	1		
164	Pilas.	779	780	108	1	1		
165	Pilas.	767	768	108	1	1		
166	Pilas.	755	756	108	1	1		
167	Pilas.	739	740	108	1	1		
168	Pilas.	723	724	108	1	1		
169	Pilas.	707	708	108	1	1		
170	Pilas.	691	692	108	1	1		
171	Pilas.	675	676	108	1	1		
172	Pilas.	584	628	108	1	1		
173	Pilas.	527	555	108	1	1		
174	Pilas.	670	674	108	1	1		
175	Pilas.	834	527	108	1	1		
176	Trave	895	654	159	3	1	000001	000001
177	Pilas.	526	525	108	5	1		
178	Pilas.	551	550	108	5	1		
179	Trave	580	886	159	3	1		
180	Trave	596	882	159	3	1		
181	Trave	470	882	159	6	1		
182	Trave	882	886	159	6	1		
183	Trave	886	953	159	6	1		
184	Trave	186	518	159	7	1		
185	Trave	518	516	159	7	1		
186	Trave	84	516	159	7	1		
187	Trave	516	226	159	7	1		
188	Trave	518	214	159	7	1		
189	Trave	561	819	159	3	1		
190	Trave	186	84	159	8	1	000001	000001
191	Pilas.	7	556	108	1	1		
192	Pilas.	556	559	108	1	1		
193	Pilas.	17	19	108	1	1		
194	Pilas.	33	35	108	1	1		
195	Pilas.	49	51	108	1	1		
196	Pilas.	65	67	108	1	1		
197	Pilas.	81	83	108	1	1		
198	Pilas.	97	99	108	1	1		
199	Pilas.	223	225	108	1	1		
200	Pilas.	211	213	108	1	1		
201	Pilas.	199	201	108	1	1		
202	Pilas.	183	185	108	1	1		
203	Pilas.	167	169	108	1	1		
204	Pilas.	151	153	108	1	1		
205	Pilas.	135	137	108	1	1		
206	Pilas.	119	121	108	1	1		
207	Pilas.	104	107	108	1	1		
208	Pilas.	407	409	108	1	1		
209	Pilas.	523	524	108	1	1		
210	Pilas.	525	528	108	5	1		
211	Pilas.	550	552	108	5	1		
212	Pilas.	559	561	108	1	1		
213	Pilas.	19	20	108	1	1		
214	Pilas.	35	36	108	1	1		
215	Pilas.	51	52	108	1	1		
216	Pilas.	67	68	108	1	1		
217	Pilas.	83	84	108	1	1		
218	Pilas.	99	100	108	1	1		
219	Pilas.	225	226	108	1	1		
220	Pilas.	213	214	108	1	1		
221	Pilas.	201	202	108	1	1		
222	Pilas.	185	186	108	1	1		
223	Pilas.	169	170	108	1	1		
224	Pilas.	153	154	108	1	1		
225	Pilas.	137	138	108	1	1		
226	Pilas.	121	122	108	1	1		
227	Pilas.	107	109	108	1	1		
228	Pilas.	409	410	108	1	1		
229	Pilas.	524	520	108	1	1		
230	Pilas.	528	529	108	5	1		
231	Pilas.	552	553	108	5	1		
232	Pilas.	529	909	108	5	1		

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233	Pilas.	553	253	108	5	1		
234	Pilas.	909	916	108	5	1		
235	Pilas.	253	564	108	5	1		
236	Pilas.	916	919	108	5	1		
237	Pilas.	564	568	108	5	1		
238	Trave	178	968	159	8	1	000001	
239	Trave	968	940	159	8	1		
240	Trave	940	76	159	8	1		000001
241	Pilas.	1	2	108	1	1		
242	Pilas.	2	5	108	1	1		
243	Pilas.	5	7	108	1	1		

MODELLAZIONE DELLA STRUTTURA: ELEMENTI SOLAIO-PANNELLO

LEGENDA TABELLA DATI SOLAI-PANNELLI

Il programma utilizza per la modellazione elementi a tre o più nodi denominati in generale solaio o pannello.

Ogni elemento solaio-pannello è individuato da una poligonale di nodi 1,2, ..., N.

L'elemento solaio è utilizzato in primo luogo per la modellazione dei carichi agenti sugli elementi strutturali. In secondo luogo può essere utilizzato per la corretta ripartizione delle forze orizzontali agenti nel proprio piano. L'elemento balcone è derivato dall'elemento solaio.

I carichi agenti sugli elementi solaio, raccolti in un archivio, sono direttamente assegnati agli elementi utilizzando le informazioni raccolte nell'archivio (es. i coefficienti combinatori). La tabella seguente riporta i dati utilizzati per la definizione dei carichi e delle masse.

L'elemento pannello è utilizzato solo per l'applicazione dei carichi, quali pesi delle tamponature o spinte dovute al vento o terre. In questo caso i carichi sono applicati in analogia agli altri elementi strutturali (si veda il cap. SCHEMATIZZAZIONE DEI CASI DI CARICO).

Id.Arch.	Identificativo dell' archivio
Tipo	Tipo di carico <i>Variab.</i> Carico variabile generico <i>Var. rid.</i> Carico variabile generico con riduzione in funzione dell' area (c.5.5. ...) <i>Neve</i> Carico di neve
G1k	carico permanente (comprensivo del peso proprio)
G2k	carico permanente non strutturale e non compiutamente definito
Qk	carico variabile
Fatt. A	fattore di riduzione del carico variabile (0.5 o 0.75) per tipo "Var.rid."
S sis.	fattore di riduzione del carico variabile per la definizione delle masse sismiche per D.M. 96 (vedi NOTA sul capitolo "normativa di riferimento")
Psi 0	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: <i>per valore raro</i>
Psi 1	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: <i>per valore frequente</i>
Psi 2	Coefficiente combinatorio dei valori caratteristici delle azioni variabili: <i>per valore quasi permanente</i>
Psi S 2	Coefficiente di combinazione che fornisce il valore quasi-permanente dell'azione variabile: <i>per la definizione delle masse sismiche</i>
Fatt. Fi	Coefficiente di correlazione dei carichi per edifici

Ogni elemento è caratterizzato da un insieme di proprietà riportate in tabella che ne completano la modellazione. In particolare per ogni elemento viene indicato in tabella:

Elem	numero dell'elemento
Tipo	codice di comportamento <i>S</i> elemento utilizzato solo per scarico <i>C</i> elemento utilizzato per scarico e per modellazione piano rigido <i>P</i> elemento utilizzato come pannello <i>M</i> scarico monodirezionale

B scarico bidirezionale	
Id.Arch.	Identificativo dell' archivio
Mat	codice del materiale assegnato all'elemento
Spessore	spessore dell'elemento (costante)
Orditura	angolo (rispetto all'asse X) della direzione dei travetti principali
Gk	carico permanente solaio (comprensivo del peso proprio)
Qk	carico variabile solaio
Nodi	numero dei nodi che definiscono l'elemento (5 per riga)

Nel caso in cui si sia proceduto alla progettazione dei solai con le tensioni ammissibili vengono riportate le massime tensioni nell'elemento (massima compressione nel calcestruzzo, massima tensione nell'acciaio, massima tensione tangenziale); nel caso in cui si sia proceduto alla progettazione con il metodo degli stati limite vengono riportati il rapporto x/d e le verifiche per sollecitazioni proporzionali nonché le verifiche in esercizio.

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	numero identificativo dell'elemento
Stato	Codici di verifica relativi alle tensioni normali e alle tensioni tangenziali
Note	Viene riportato il codice relativo alla sezione(s) e relativo al materiale(m);
Pos.	Ascissa del punto di verifica
F ist, F infi	Frecce istantanee e a tempo infinito
Momento	Momento flettente
Taglio	Sollecitazione di taglio
Af inf.	Area di armatura longitudinale posta all'intradosso della trave
Af sup.	Area di armatura longitudinale posta all'estradosso della trave
AfV	Area dell'armatura atta ad assorbire le azioni di taglio
Beff	Base della sezione di cls per l'assorbimento del taglio
simboli utilizzati con il metodo delle tensioni ammissibili:	
sc max	Massima tensione di compressione del calcestruzzo
sf max	Massima tensione nell'acciaio
tau max	Massima tensione tangenziale nel cls
simboli utilizzati con il metodo degli stati limite:	
x/d	rapporto tra posizione dell'asse neutro e altezza utile alla rottura della sezione (per sola flessione)
verif.	rapporto S_d/S_u con sollecitazioni ultime proporzionali: valore minore o uguale a 1 per verifica positiva
Verif.V	rapporto S_d/S_u con sollecitazioni taglianti proporzionali valore minore o uguale a 1 per verifica positiva
rRfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni rare [normalizzato a 1]
rFfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni frequenti [normalizzato a 1]
rPfck	rapporto tra la massima compressione nel calcestruzzo e la tensione f_{ck} in combinazioni quasi permanenti [normalizzato a 1]
rRfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni frequenti [normalizzato a 1]
rFyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni rare [normalizzato a 1]
rPfyk	rapporto tra la massima tensione nell'acciaio e la tensione f_{yk} in combinazioni quasi permanenti [normalizzato a 1]
wR	apertura caratteristica delle fessure in combinazioni rare [mm]

wF	apertura caratteristica delle fessure in combinazioni frequenti [mm]
wP	apertura caratteristica delle fessure in combinazioni quasi permanenti [mm]

Nel caso in cui si sia proceduto alla verifica delle tamponature secondo il D.M. 17.01.2018 - §7.2.3 viene riportata una tabella riassuntiva delle verifiche degli elementi pannello. La verifica confronta i momenti sollecitanti indotti dal sisma con i momenti resistenti, secondo tre ipotesi, due basate sulla resistenza a pressoflessione della tamponatura ed una basata sul cinematismo a seguito della formazione di tre cerniere plastiche sulla tamponatura (rif. Ufficio di Vigilanza sulle Costruzioni, Provincia di Terni).

Qualora la tamponatura sia di tipo antiespulsione (nelle due possibili varianti ordinaria o armata) viene condotta una verifica con meccanismo ad arco con degrado di resistenza. La verifica confronta le pressioni sollecitanti indotte dal sisma con le pressioni resistenti che la tamponatura sviluppa attraverso il meccanismo ad arco. La verifica considera anche il degrado di resistenza dovuto al danneggiamento nel piano della tamponatura.

Per quest'ultima tamponatura sono disponibili, in funzione del materiale impiegato (materiale [52] o materiale [53]):

- **Tamponatura Antiespulsione ordinaria Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova. Utilizzabile per il materiale [52].
- **Tamponatura Antiespulsione armata Poroton® Cis Edil** sp.30 cm; con metodo di verifica per meccanismo ad arco con degrado di resistenza, sviluppato attraverso i risultati di un progetto di ricerca sperimentale condotto dall'Università degli Studi di Padova. Utilizzabile per il materiale [53].

La verifica è stata calibrata sulla base di prove sperimentali sul sistema di Tamponatura Antiespulsione anche in presenza di aperture.

(rif. Rapporti di Prova redatti dal Dipartimento ICEA - Università degli Studi di Padova di test sperimentali condotti sul sistema Tamponatura Antiespulsione di Cis Edil)

In particolare i simboli utilizzati in tabella assumono il seguente significato:

Elem.	Numero identificativo dell'elemento
Stato	Codice di verifica
Ver. c.c.	Verifica nell'ipotesi di trave appoggiata con carico concentrato in mezzeria
Ver. c.d.	Verifica nell'ipotesi di trave appoggiata con carico distribuito
Ver. c.cin.	Verifica nell'ipotesi di cinematismo con formazione di cerniere plastiche in appoggio e mezzeria
Ver. CIS	Rapporto p_a/p_r (valore minore o uguale a 1 per verifica positiva)
Z	Quota del baricentro dell'elemento
T1	Periodo proprio dell'edificio nella direzione di interesse (ortogonale al pannello)
Ta	Periodo proprio della parete
Sa	Accelerazione massima, adimensionalizzata allo SLV
p_a	Pressione sulla parete causata dall'azione sismica
p_r	Pressione resistente del meccanismo ad arco
Drift	Spostamento relativo interpiano allo SLV valutato secondo il D.M. 14.01.2018 - § 7.3.3.3
Beta a	Coef. riduttivo per tener conto del danneggiamento del piano dipendente dallo spostamento, ottenuto sperimentalmente

ID Arch.	Tipo	G1k kN/ m2	G2k kN/ m2	Qk kN/ m2	Fatt. A	s sis.	Psi 0	Psi 1	Psi 2	Psi S 2	Fatt. Fi
1	Variab.	3.00	2.00	2.00		1.00	0.70	0.50	0.30	0.30	1.00
2	Variab.	2.10	0.50	1.00		1.00	0.50	0.20	0.0	0.0	1.00

INGEGNERE

3	Variab.	3.00	0.50	1.00		1.00	0.50	0.20	0.0	0.0	1.00
4	Variab.	3.00	0.10	1.00		1.00	0.50	0.20	0.0	0.0	1.00

Elem.	Tipo	ID Arch.	Mat.	Spessore	Orditura	G1k kN/ m2	G2k kN/ m2	Qk kN/ m2	Nodo 1/6..	Nodo 2/7..	Nodo 3/8..	Nodo..	Nodo..
1	CM	1	m=158	5.0	90.0	3.00	2.00	2.00	516 96	226 95	230 102	234 88	100 84
2	CM	1	m=158	5.0	90.0	3.00	2.00	2.00	518 226	214 516	218	927	222
3	CM	1	m=158	5.0	90.0	3.00	2.00	2.00	190 210	194 214	198 518	202 186	206
4	SM	1	m=158	1.0	0.0	3.00	2.00	2.00	178 76	182	186	84	80
5	SM	2	m=158	5.0	90.0	2.10	0.50	1.00	562 582 839 819	566 586 835 561	570 590 831	574 847 827	578 843 823
6	CM	1	m=158	5.0	90.0	3.00	2.00	2.00	238 370 330 310 290 270 7 24 44 64 84 100	242 366 326 306 286 266 8 28 48 68 88	358 365 322 302 282 262 12 32 52 72 102	378 382 318 298 278 258 16 36 56 76 95	374 334 314 294 274 254 20 40 60 80 96
7	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	686 566 864	730 562 936	746 561 643	574 876 808	570 652
8	SM	2	m=12	5.0	90.0	2.10	0.50	1.00	752 732 944	748 568 934	744 522 919	740 962 756	736 952
9	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	746 666 574	730 590	686 586	616 582	660 578
10	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	686 684 616	714 688	726 692	676 646	680 636
11	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	636 704 616	646 708	692 801	696 798	700 762
12	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	762 598 616	805 594	807 590	606 666	602 660
13	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	807 854 606	805 622	762 618	818 614	838 610
14	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	762 716 818	798 720	801 724	708 836	712 826
15	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	854 913 622	838 638	818 634	880 630	898 626
16	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	818 732 880	826 736	836 740	724 896	728 894
17	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	913 834 650	898 820 649	880 814 656	925 830 642	804 654 638
18	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	880 748 888	894 752 931	896 756 802	740 932 925	744 860
19	SM	2	m=12	5.0	90.0	2.10	0.50	1.00	594 614 634 650 887 867 847	598 618 638 654 883 863 590	602 622 642 895 879 859	606 626 656 891 875 855	610 630 649 935 871 851
20	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	895 800	654 908	792 904	796 900	912
21	SM	2	m=12	5.0	0.0	2.10	0.50	1.00	840 663 726	852 664 714	828 668 686	923 672 808	856 676
22	CM	3	m=158	5.0	0.0	3.00	0.50	1.00	953	957	961	965	969

INGEGNERE

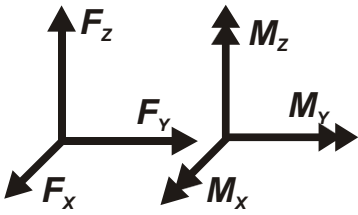
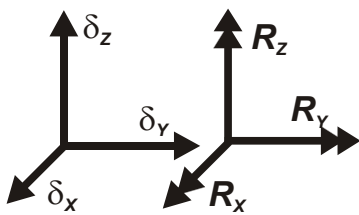
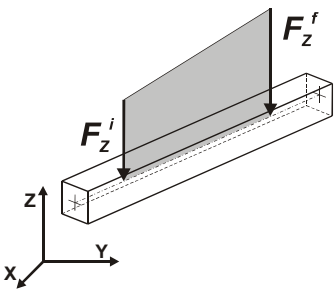
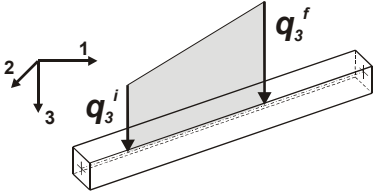
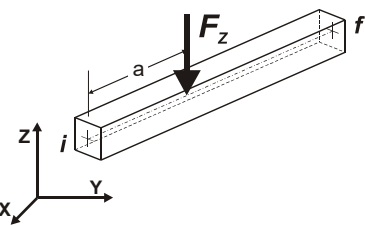
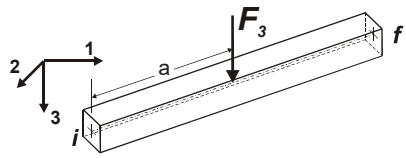
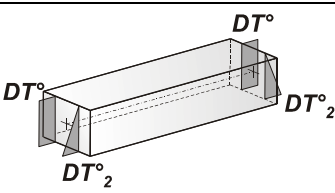
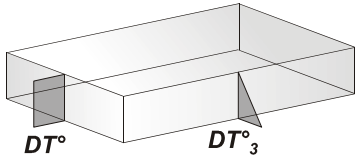
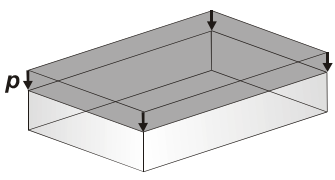
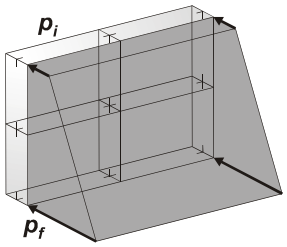
23	CM	3 m=158	5.0	0.0	3.00	0.50	1.00	878 874 886	874 866	886 862	858	882
24	CM	3 m=158	5.0	0.0	3.00	0.50	1.00	850 474	846 470	486 882	482 858	478
25	CM	3 m=158	5.0	0.0	3.00	0.50	1.00	886 902	580 949	576 953	941	945
26	CM	3 m=158	5.0	0.0	3.00	0.50	1.00	882 886	596	592	588	580
27	CM	3 m=158	5.0	0.0	3.00	0.50	1.00	882 454	470 608	466 604	462 596	458
28	SM	2 m=158	5.0	90.0	2.10	0.50	1.00	561	819	815		
29	SM	4 m=158	1.0	0.0	3.00	0.10	1.00	529 238 222 206	974 100 927 202	973 234 218	246 230 214	358 226 210

MODELLAZIONE DELLE AZIONI

LEGENDA TABELLA DATI AZIONI

Il programma consente l'uso di diverse tipologie di carico (azioni). Le azioni utilizzate nella modellazione sono individuate da una sigla identificativa ed un codice numerico (gli elementi strutturali richiamano quest'ultimo nella propria descrizione). Per ogni azione applicata alla struttura viene di riportato il codice, il tipo e la sigla identificativa. Le tabelle successive dettagliano i valori caratteristici di ogni azione in relazione al tipo. Le tabelle riportano infatti i seguenti dati in relazione al tipo:

1	carico concentrato nodale 6 dati (forza F_x , F_y , F_z , momento M_x , M_y , M_z)
2	spostamento nodale impresso 6 dati (spostamento T_x , T_y , T_z , rotazione R_x , R_y , R_z)
3	carico distribuito globale su elemento tipo trave 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di inizio carico) 7 dati (f_x , f_y , f_z , m_x , m_y , m_z , ascissa di fine carico)
4	carico distribuito locale su elemento tipo trave 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di inizio carico) 7 dati (f_1 , f_2 , f_3 , m_1 , m_2 , m_3 , ascissa di fine carico)
5	carico concentrato globale su elemento tipo trave 7 dati (F_x , F_y , F_z , M_x , M_y , M_z , ascissa di carico)
6	carico concentrato locale su elemento tipo trave 7 dati (F_1 , F_2 , F_3 , M_1 , M_2 , M_3 , ascissa di carico)
7	variazione termica applicata ad elemento tipo trave 7 dati (variazioni termiche: uniforme, media e differenza in altezza e larghezza al nodo iniziale e finale)
8	carico di pressione uniforme su elemento tipo piastra 1 dato (pressione)
9	carico di pressione variabile su elemento tipo piastra 4 dati (pressione, quota, pressione, quota)
10	variazione termica applicata ad elemento tipo piastra 2 dati (variazioni termiche: media e differenza nello spessore)
11	carico variabile generale su elementi tipo trave e piastra 1 dato descrizione della tipologia 4 dati per segmento (posizione, valore, posizione, valore) la tipologia precisa l'ascissa di definizione, la direzione del carico, la modalità di carico e la larghezza d'influenza per gli elementi tipo trave
12	gruppo di carichi con impronta su piastra 9 dati (numero di ripetizioni in direzione X e Y, valore di ciascun carico, posizione centrale del primo, dimensioni dell'impronta, interasse tra i carichi)

 Carico concentrato nodale	 Spostamento impresso
 Carico distribuito globale	 Carico distribuito locale
 Carico concentrato globale	 Carico concentrato locale
 Carico termico 2D	 Carico termico 3D
 Carico pressione uniforme	 Carico pressione variabile

SCHEMATIZZAZIONE DEI CASI DI CARICO

LEGENDA TABELLA CASI DI CARICO

Il programma consente l'applicazione di diverse tipologie di casi di carico.

Sono previsti i seguenti 11 tipi di casi di carico:

	Sigla	Tipo	Descrizione
1	Ggk	A	caso di carico comprensivo del peso proprio struttura
2	Gk	NA	caso di carico con azioni permanenti
3	Qk	NA	caso di carico con azioni variabili
4	Gsk	A	caso di carico comprensivo dei carichi permanenti sui solai e sulle coperture
5	Qsk	A	caso di carico comprensivo dei carichi variabili sui solai
6	Qnk	A	caso di carico comprensivo dei carichi di neve sulle coperture
7	Qtk	SA	caso di carico comprensivo di una variazione termica agente sulla struttura
8	Qvk	NA	caso di carico comprensivo di azioni da vento sulla struttura
9	Esk	SA	caso di carico sismico con analisi statica equivalente
10	Edk	SA	caso di carico sismico con analisi dinamica
11	Etk	NA	caso di carico comprensivo di azioni derivanti dall' incremento di spinta delle terre in condizione sismica
12	Pk	NA	caso di carico comprensivo di azioni derivanti da coazioni, cedimenti e precompressioni

Sono di tipo automatico A (ossia non prevedono introduzione dati da parte dell'utente) i seguenti casi di carico: 1-Ggk; 4-Gsk; 5-Qsk; 6-Qnk.

Sono di tipo semi-automatico SA (ossia prevedono una minima introduzione dati da parte dell'utente) i seguenti casi di carico:

7-Qtk, in quanto richiede solo il valore della variazione termica;

9-Esk e 10-Edk, in quanto richiedono il valore dell'angolo di ingresso del sisma e l'individuazione dei casi di carico partecipanti alla definizione delle masse.

Sono di tipo non automatico NA ossia prevedono la diretta applicazione di carichi generici agli elementi strutturali (si veda il precedente punto Modellazione delle Azioni) i restanti casi di carico.

Nella tabella successiva vengono riportati i casi di carico agenti sulla struttura, con l'indicazione dei dati relativi al caso di carico stesso:

Numero Tipo e Sigla identificativa, Valore di riferimento del caso di carico (se previsto).

In successione, per i casi di carico non automatici, viene riportato l'elenco di nodi ed elementi direttamente caricati con la sigla identificativa del carico.

Per i casi di carico di tipo sismico (9-Esk e 10-Edk), viene riportata la tabella di definizione delle masse: per ogni caso di carico partecipante alla definizione delle masse viene indicata la relativa aliquota (partecipazione) considerata. Si precisa che per i caso di carico 5-Qsk e 6-Qnk la partecipazione è prevista localmente per ogni elemento solaio o copertura presente nel modello (si confronti il valore Sksol nel capitolo relativo agli elementi solaio) e pertanto la loro partecipazione è di norma pari a uno.

CDC	Tipo	Sigla Id	Note
1	Ggk	CDC=Ggk (peso proprio della struttura)	
2	Gsk	CDC=G1sk (permanente solai-coperture)	

CDC	Tipo	Sigla Id	Note
3	Gsk	CDC=G2sk (permanente solai-coperture n.c.d.)	
4	Qsk	CDC=Qsk (variabile solai)	
5	Qsk	CDC=Qsk (variabile solai)	
6	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. +)	partecipazione:1.00 per 1 CDC=Ggk (peso proprio della struttura)
			partecipazione:1.00 per 2 CDC=G1sk (permanente solai-coperture)
			partecipazione:1.00 per 3 CDC=G2sk (permanente solai-coperture n.c.d.)
			partecipazione:1.00 per 4 CDC=Qsk (variabile solai)
			partecipazione:1.00 per 5 CDC=Qsk (variabile solai)
7	Edk	CDC=Ed (dinamico SLU) alfa=0.0 (ecc. -)	come precedente CDC sismico
8	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. +)	come precedente CDC sismico
9	Edk	CDC=Ed (dinamico SLU) alfa=90.00 (ecc. -)	come precedente CDC sismico
10	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. +)	come precedente CDC sismico
11	Edk	CDC=Ed (dinamico SLD) alfa=0.0 (ecc. -)	come precedente CDC sismico
12	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. +)	come precedente CDC sismico
13	Edk	CDC=Ed (dinamico SLD) alfa=90.00 (ecc. -)	come precedente CDC sismico

DEFINIZIONE DELLE COMBINAZIONI

LEGENDA TABELLA COMBINAZIONI DI CARICO

Il programma combina i diversi tipi di casi di carico (CDC) secondo le regole previste dalla normativa vigente.

Le combinazioni previste sono destinate al controllo di sicurezza della struttura ed alla verifica degli spostamenti e delle sollecitazioni.

La prima tabella delle combinazioni riportata di seguito comprende le seguenti informazioni:

Numero, Tipo, Sigla identificativa. Una seconda tabella riporta il peso nella combinazione assunto per ogni caso di carico.

Ai fini delle verifiche degli stati limite si definiscono le seguenti combinazioni delle azioni:

Combinazione fondamentale SLU

$$\gamma G1 \cdot G1 + \gamma G2 \cdot G2 + \gamma P \cdot P + \gamma Q1 \cdot Qk1 + \gamma Q2 \cdot \psi 02 \cdot Qk2 + \gamma Q3 \cdot \psi 03 \cdot Qk3 + \dots$$

Combinazione caratteristica (rara) SLE

$$G1 + G2 + P + Qk1 + \psi 02 \cdot Qk2 + \psi 03 \cdot Qk3 + \dots$$

Combinazione frequente SLE

$$G1 + G2 + P + \psi 11 \cdot Qk1 + \psi 22 \cdot Qk2 + \psi 23 \cdot Qk3 + \dots$$

Combinazione quasi permanente SLE

$$G1 + G2 + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \psi 23 \cdot Qk3 + \dots$$

Combinazione sismica, impiegata per gli stati limite ultimi e di esercizio connessi all'azione sismica E

$$E + G1 + G2 + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \dots$$

Combinazione eccezionale, impiegata per gli stati limite connessi alle azioni eccezionali

$$G1 + G2 + Ad + P + \psi 21 \cdot Qk1 + \psi 22 \cdot Qk2 + \dots$$

Dove:

NTC 2018 Tabella 2.5.1

Destinazione d'uso/azione	$\psi 0$	$\psi 1$	$\psi 2$
Categoria A residenziali	0,70	0,50	0,30
Categoria B uffici	0,70	0,50	0,30
Categoria C ambienti suscettibili di affollamento	0,70	0,70	0,60
Categoria D ambienti ad uso commerciale	0,70	0,70	0,60
Categoria E biblioteche, archivi, magazzini,...	1,00	0,90	0,80
Categoria F Rimesse e parcheggi (autoveicoli $\leq 30kN$)	0,70	0,70	0,60
Categoria G Rimesse e parcheggi (autoveicoli $> 30kN$)	0,70	0,50	0,30
Categoria H Coperture	0,00	0,00	0,00
Vento	0,60	0,20	0,00
Neve a quota $\leq 1000\text{ m}$	0,50	0,20	0,00
Neve a quota $> 1000\text{ m}$	0,70	0,50	0,20
Variazioni Termiche	0,60	0,50	0,00

Nelle verifiche possono essere adottati in alternativa due diversi approcci progettuali:

- per l'approccio 1 si considerano due diverse combinazioni di gruppi di coefficienti di sicurezza parziali per le azioni, per i materiali e per la resistenza globale (combinazione 1 con coefficienti $A1$ e combinazione 2 con coefficienti $A2$),

- per l'approccio 2 si definisce un'unica combinazione per le azioni, per la resistenza dei materiali e per la resistenza globale (con coefficienti A1).

NTC 2018 Tabella 2.6.I

		Coefficiente γ_f	EQU	A1	A2
<i>Carichi permanenti</i>	<i>Favorevoli</i>	γ_{G1}	0,9	1,0	1,0
	<i>Sfavorevoli</i>		1,1	1,3	1,0
<i>Carichi permanenti non strutturali</i> (Non compiutamente definiti)	<i>Favorevoli</i>	γ_{G2}	0,8	0,8	0,8
	<i>Sfavorevoli</i>		1,5	1,5	1,3
<i>Carichi variabili</i>	<i>Favorevoli</i>	γ_{Qi}	0,0 1,5	0,0 1,5	0,0 1,3

Cmb	Tipo	Sigla Id	effetto P-delta
1	SLU	Comb. SLU A1 1	
2	SLU	Comb. SLU A1 2	
3	SLU	Comb. SLU A1 3	
4	SLU	Comb. SLU A1 4	
5	SLU	Comb. SLU A1 5	
6	SLU	Comb. SLU A1 6	
7	SLU	Comb. SLU A1 7	
8	SLU	Comb. SLU A1 8	
9	SLU	Comb. SLU A1 9	
10	SLU	Comb. SLU A1 10	
11	SLU	Comb. SLU A1 11	
12	SLU	Comb. SLU A1 12	
13	SLU	Comb. SLU A1 13	
14	SLU	Comb. SLU A1 14	
15	SLU	Comb. SLU A1 (SLV sism.) 15	
16	SLU	Comb. SLU A1 (SLV sism.) 16	
17	SLU	Comb. SLU A1 (SLV sism.) 17	
18	SLU	Comb. SLU A1 (SLV sism.) 18	
19	SLU	Comb. SLU A1 (SLV sism.) 19	
20	SLU	Comb. SLU A1 (SLV sism.) 20	
21	SLU	Comb. SLU A1 (SLV sism.) 21	
22	SLU	Comb. SLU A1 (SLV sism.) 22	
23	SLU	Comb. SLU A1 (SLV sism.) 23	
24	SLU	Comb. SLU A1 (SLV sism.) 24	
25	SLU	Comb. SLU A1 (SLV sism.) 25	
26	SLU	Comb. SLU A1 (SLV sism.) 26	
27	SLU	Comb. SLU A1 (SLV sism.) 27	
28	SLU	Comb. SLU A1 (SLV sism.) 28	
29	SLU	Comb. SLU A1 (SLV sism.) 29	
30	SLU	Comb. SLU A1 (SLV sism.) 30	
31	SLU	Comb. SLU A1 (SLV sism.) 31	
32	SLU	Comb. SLU A1 (SLV sism.) 32	
33	SLU	Comb. SLU A1 (SLV sism.) 33	
34	SLU	Comb. SLU A1 (SLV sism.) 34	
35	SLU	Comb. SLU A1 (SLV sism.) 35	
36	SLU	Comb. SLU A1 (SLV sism.) 36	
37	SLU	Comb. SLU A1 (SLV sism.) 37	
38	SLU	Comb. SLU A1 (SLV sism.) 38	
39	SLU	Comb. SLU A1 (SLV sism.) 39	
40	SLU	Comb. SLU A1 (SLV sism.) 40	
41	SLU	Comb. SLU A1 (SLV sism.) 41	
42	SLU	Comb. SLU A1 (SLV sism.) 42	
43	SLU	Comb. SLU A1 (SLV sism.) 43	
44	SLU	Comb. SLU A1 (SLV sism.) 44	
45	SLU	Comb. SLU A1 (SLV sism.) 45	
46	SLU	Comb. SLU A1 (SLV sism.) 46	
47	SLD(sis)	Comb. SLE (SLD Danno sism.) 47	
48	SLD(sis)	Comb. SLE (SLD Danno sism.) 48	
49	SLD(sis)	Comb. SLE (SLD Danno sism.) 49	
50	SLD(sis)	Comb. SLE (SLD Danno sism.) 50	

INGEGNERE

Cmb	Tipo	Sigla Id	effetto P-delta
51	SLD(sis)	Comb. SLE (SLD Danno sism.) 51	
52	SLD(sis)	Comb. SLE (SLD Danno sism.) 52	
53	SLD(sis)	Comb. SLE (SLD Danno sism.) 53	
54	SLD(sis)	Comb. SLE (SLD Danno sism.) 54	
55	SLD(sis)	Comb. SLE (SLD Danno sism.) 55	
56	SLD(sis)	Comb. SLE (SLD Danno sism.) 56	
57	SLD(sis)	Comb. SLE (SLD Danno sism.) 57	
58	SLD(sis)	Comb. SLE (SLD Danno sism.) 58	
59	SLD(sis)	Comb. SLE (SLD Danno sism.) 59	
60	SLD(sis)	Comb. SLE (SLD Danno sism.) 60	
61	SLD(sis)	Comb. SLE (SLD Danno sism.) 61	
62	SLD(sis)	Comb. SLE (SLD Danno sism.) 62	
63	SLD(sis)	Comb. SLE (SLD Danno sism.) 63	
64	SLD(sis)	Comb. SLE (SLD Danno sism.) 64	
65	SLD(sis)	Comb. SLE (SLD Danno sism.) 65	
66	SLD(sis)	Comb. SLE (SLD Danno sism.) 66	
67	SLD(sis)	Comb. SLE (SLD Danno sism.) 67	
68	SLD(sis)	Comb. SLE (SLD Danno sism.) 68	
69	SLD(sis)	Comb. SLE (SLD Danno sism.) 69	
70	SLD(sis)	Comb. SLE (SLD Danno sism.) 70	
71	SLD(sis)	Comb. SLE (SLD Danno sism.) 71	
72	SLD(sis)	Comb. SLE (SLD Danno sism.) 72	
73	SLD(sis)	Comb. SLE (SLD Danno sism.) 73	
74	SLD(sis)	Comb. SLE (SLD Danno sism.) 74	
75	SLD(sis)	Comb. SLE (SLD Danno sism.) 75	
76	SLD(sis)	Comb. SLE (SLD Danno sism.) 76	
77	SLD(sis)	Comb. SLE (SLD Danno sism.) 77	
78	SLD(sis)	Comb. SLE (SLD Danno sism.) 78	

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
1	1.30	1.30	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
2	1.30	1.30	1.50	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
3	1.30	1.30	1.50	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
4	1.30	1.30	1.50	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
5	1.00	1.00	0.80	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
6	1.00	1.00	0.80	0.0	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
7	1.00	1.00	0.80	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
8	1.00	1.00	0.80	1.50	0.75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
9	1.30	1.30	1.50	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
10	1.30	1.30	1.50	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
11	1.30	1.30	1.50	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
12	1.00	1.00	0.80	0.0	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
13	1.00	1.00	0.80	1.05	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
14	1.00	1.00	0.80	1.05	1.50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	
15	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	
16	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	
17	1.00	1.00	1.00	0.30	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	0.0	
18	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	0.0	
19	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	
20	1.00	1.00	1.00	0.30	0.0	-1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	
21	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.0	-0.30	0.0	0.0	0.0	0.0	
22	1.00	1.00	1.00	0.30	0.0	1.00	0.0	0.0	0.30	0.0	0.0	0.0	0.0	
23	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	-0.30	0.0	0.0	0.0	0.0	0.0	
24	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.30	0.0	0.0	0.0	0.0	0.0	
25	1.00	1.00	1.00	0.30	0.0	0.0	1.00	-0.30	0.0	0.0	0.0	0.0	0.0	
26	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.30	0.0	0.0	0.0	0.0	0.0	
27	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.0	-0.30	0.0	0.0	0.0	0.0	
28	1.00	1.00	1.00	0.30	0.0	0.0	-1.00	0.0	0.30	0.0	0.0	0.0	0.0	
29	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.0	-0.30	0.0	0.0	0.0	0.0	
30	1.00	1.00	1.00	0.30	0.0	0.0	1.00	0.0	0.30	0.0	0.0	0.0	0.0	
31	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	
32	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	
33	1.00	1.00	1.00	0.30	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	0.0	
34	1.00	1.00	1.00	0.30	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	0.0	
35	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	-1.00	0.0	0.0	0.0	0.0	0.0	
36	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	1.00	0.0	0.0	0.0	0.0	0.0	
37	1.00	1.00	1.00	0.30	0.0	0.0	0.30	-1.00	0.0	0.0	0.0	0.0	0.0	
38	1.00	1.00	1.00	0.30	0.0	0.0	0.30	1.00	0.0	0.0	0.0	0.0	0.0	
39	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	
40	1.00	1.00	1.00	0.30	0.0	-0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	
41	1.00	1.00	1.00	0.30	0.0	0.30	0.0	0.0	-1.00	0.0	0.0	0.0	0.0	
42	1.00	1.00	1.00	0.30	0.0	0.30	0.0	0.0	1.00	0.0	0.0	0.0	0.0	
43	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	0.0	-1.00	0.0	0.0	0.0	0.0	

INGEGNERE

Cmb	CDC 1/15...	CDC 2/16...	CDC 3/17...	CDC 4/18...	CDC 5/19...	CDC 6/20...	CDC 7/21...	CDC 8/22...	CDC 9/23...	CDC 10/24...	CDC 11/25...	CDC 12/26...	CDC 13/27...	CDC 14/28...
44	1.00	1.00	1.00	0.30	0.0	0.0	-0.30	0.0	1.00	0.0	0.0	0.0	0.0	
45	1.00	1.00	1.00	0.30	0.0	0.0	0.30	0.0	-1.00	0.0	0.0	0.0	0.0	
46	1.00	1.00	1.00	0.30	0.0	0.0	0.30	0.0	1.00	0.0	0.0	0.0	0.0	
47	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	0.0	
48	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	0.0	
49	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	0.0	
50	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	0.0	
51	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	-0.30	
52	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.0	0.30	
53	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	-0.30	
54	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.0	0.30	
55	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	-0.30	0.0	
56	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.30	0.0	
57	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	-0.30	0.0	
58	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.30	0.0	
59	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	-0.30	
60	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-1.00	0.0	0.30	
61	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	-0.30	
62	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	1.00	0.0	0.30	
63	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	0.0	
64	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	0.0	
65	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	0.0	
66	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	0.0	
67	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	-1.00	0.0	
68	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	1.00	0.0	
69	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	-1.00	0.0	
70	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	1.00	0.0	
71	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	-1.00	
72	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	0.0	1.00	
73	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	-1.00	
74	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.30	0.0	0.0	1.00	
75	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	-1.00	
76	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	-0.30	0.0	1.00	
77	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	-1.00	
78	1.00	1.00	1.00	0.30	0.0	0.0	0.0	0.0	0.0	0.0	0.30	0.0	1.00	

VERIFICHE PER ELEMENTI IN ACCIAIO

LEGENDA TABELLA VERIFICHE PER ELEMENTI IN ACCIAIO

Il programma consente la verifica dei seguenti tipi di elementi:

1. **aste** 2. **travi** 3. **pilastr**

L'esito delle verifiche è espresso con un codice come di seguito indicato

- Ok:** verifica con esito positivo
NV: verifica con esito negativo
Nr: verifica non richiesta.

Per comodità gli elementi vengono raggruppati in tabelle in relazione al tipo.

Ai fini delle verifiche (come da D.M. 17 Gennaio 2018 e circolare 21 Gennaio 2019 n.7) i tipi elementi differiscono per i seguenti aspetti:

Verifica	Aste	Travi	Pilastr
4.2.3.1 Classificazione	X	X	X
4.2.4.1.2.1 Trazione	X	X	X
4.2.4.1.2.2 Compressione	X	X	X
4.2.4.1.2.4 Taglio		X	X
4.2.4.1.2.5 Torsione		X	X
Flessione, taglio e forza assiale		X	X
4.2.4.1.3.1 Aste compresse	X	X	X
4.2.4.1.3.2 Instabilità flesso-torsionale		X	X
4.2.4.1.3.3 Membrature inflesse e compresse		X	X

Ai fini delle verifiche per strutture dissipative (come da D.M. 17 Gennaio 2018 e 2018 e circolare 21 Gennaio 2019 n.7) per strutture intelaiate e a controventi concentrici) si considerano le verifiche del capitolo 4 con azioni amplificate e le verifiche del capitolo 7:

Verifica	Travi	Pilastr
4.2.4.1.2.1 Trazione	X	X
4.2.4.1.2.2 Compressione	X	X
4.2.4.1.2.4 Taglio	X	X
4.2.4.1.2.5 Torsione	X	X
Flessione, taglio e forza assiale	X	X
4.2.4.1.3.1 Aste compresse	X	X
4.2.4.1.3.2 Instabilità flesso-torsionale	X	X
4.2.4.1.3.3 Membrature inflesse e compresse	X	X
7.5.3 Sfruttamento per momento	X	
7.5.4 Sfruttamento per sforzo normale	X	
7.5.5 Sfruttamento per taglio da capacità flessionale	X	
7.5.9 Sfruttamento per taglio amplificato		X

Viene inoltre riportata la verifica della “Gerarchia delle resistenze trave-colonna” per ogni colonna, considerando piede e testa in entrambe le direzioni globali X e Y.

L'insieme delle verifiche sopra riportate è condotto sugli elementi purché dotati di sezione idonea come da tabella seguente:

Azione	SEZIONI GENERICHE	PROFILI SEMPLICI	PROFILI ACCOPPIATI
4.2.3.1 Classificazione automatica	L, doppio T, C, rettangolare cava, circolare cava	Tutti	Da profilo semplice
4.2.3.1 Classificazione di default 2	Circolare		
4.2.3.1 Classificazione di default 3	restanti		
4.2.4.1.2.1 Trazione	sì	sì	sì
4.2.4.1.2.2 Compressione	sì	sì	sì
4.2.4.1.2.4 Taglio	sì	sì	sì
4.2.4.1.2.5 Torsione	sì	sì	sì
Flessione, taglio e forza assiale	sì	sì	sì
4.2.4.1.3.1 Aste compresse	sì	sì	per elementi ravvicinati e a croce o coppie calastrellate
4.2.4.1.3.2 Travi inflesse	doppio T simmetrica	doppio T	no

Le verifiche sono riportate in tabelle con il significato sotto indicato; le verifiche sono espresse dal rapporto tra l'azione di progetto e la capacità ultima, pertanto la verifica ha esito positivo per rapporti non superiori all'unità.

Asta	Trave	Pilastr o			numero dell'elemento	
Stato					codice di verifica per resistenza, stabilità, svergolamento	
Note					sezione e materiali adottati per l'elemento	
V N					(ASTE) verifica come da par. 4.2.4.1.2 per punto (4.2.6) e (4.2.10)	
V V/T					(TRAVI E PILASTRI) verifica di resistenza come da par. 4.2.4.1.2 per azioni taglio-torsione (4.2.16 e 4.2.28)	
V N/M					(TRAVI E PILASTRI) verifica di resistenza come da par. 4.2.4.1.2 per azioni composte (4.2.33) con riduzione per taglio (4.2.40) ove richiesto	
N	M 3	M 2	V2	V3	T	sollecitazioni di interesse per la verifica
V stab					(ASTE) verifica come da par. 4.2.4.1.3.1 per punto (4.2.41)	
V stab					(TRAVI E PILASTRI) verifica come da par. 4.2.4.1.3 per punti (C4.2.32) o (C4.2.36) (membrane inflesse e compresse senza/con presenza di instabilità flesso-torsionale)	
BetaxL		B22x L	B33x L	lunghezze libere di inflessione (se indicato riferiti al piano di normale 22 o 33 rispettivamente)		
Snellezza					snellezza massima	
Classe					classe del profilo	
Chi mn					coefficiente di riduzione (della capacità) per la modalità di instabilità pertinente	
Rif. cmb					combinazioni in cui si sono rispettivamente attinti i valori di verifica più elevati	
V flst					(TRAVI E PILASTRI) verifica di stabilità come da par. 4.2.4.1.3.2 per punto (4.2.48)	
B1-1 x L					Beta1-1 x L: interasse tra i ritegni torsionali	
Chi LT					coefficiente di riduzione (della capacità) per la modalità di instabilità flesso-torsionale	
Snell adim					Valore della snellezza adimensionale, utilizzato per il controllo previsto al par. 7.5.5	

v.Omeg	Valore del rapporto capacità/domanda per l' azione di interesse (momento per travi e azione assiale per aste) utilizzato per l' amplificazione delle azioni
f.Om. N	Fattore di amplificazione delle azioni assiali per travi e colonne (prodotto di 1.1 x Omega x gamma rd materiale); utilizzato come specificato al par. 7.5.5
f.Om. T	Fattore di amplificazione delle azioni (assiali, flettenti e taglianti) per colonne (prodotto di 1.1 x Omega x gamma rd materiale); utilizzato come specificato al par. 7.5.4
V.7.5.4 M Ed	Verifica come prevista al punto 7.5.4 e valore dell' azione flettente
V.7.5.5 N Ed	Verifica come prevista al punto 7.5.5 e valore dell' azione assiale
V.7.5.6 V Ed,G V Ed,M	Verifica come prevista al punto 7.5.6 e valore dei tagli dovuti ai carichi e alla capacità
V.7.5.10 V Ed	Verifica come prevista al punto 7.5.10 e valore dell' azione di taglio
sovr. Xi (Xf, Yi, Yf)	Valore della sovreresistenza come prevista al par. 7.5.4.2 (i valori non sono normalizzati pertanto saranno maggiori uguali a gamma rd in base alla classe di duttilità)

Nel caso in cui λ_{DS} sia minore di 0.2, oppure nel caso in cui la sollecitazione di calcolo N_{Ed} sia inferiore a $0.04 N_{cr}$, gli effetti legati ai fenomeni di instabilità sono trascurati, come da paragrafo 4.2.4.1.3.1

Asta	Stato	Note	V N	N kN	V stab	N kN	Cl.	Beta x L cm	Snell. LambdaS	Chi mn	v.Omeg	Rif. cmb
1	ok	s=4,m=11	0.52	-38.3	0.59	-38.3	1	88.4	58.3	0.62	0.88	9,9
2	ok	s=4,m=11	0.32	23.6			1	127.8	84.4	0.90	0.73	9,0
3	NV	s=4,m=11	0.70	-51.5	1.39	-51.5	1	176.7	116.7	1.24	0.50	9,9
4	NV	s=4,m=11	0.70	-51.5	1.39	-51.5	1	176.7	116.7	1.24	0.50	9,9
5	ok	s=4,m=11	0.32	23.6			1	127.8	84.4	0.90	0.73	9,0
6	ok	s=4,m=11	0.52	-38.3	0.59	-38.3	1	88.4	58.3	0.62	0.88	9,9
7	ok	s=4,m=11	0.91	67.2			1	160.0	105.6	1.12	0.58	9,0
8	ok	s=4,m=11	0.55	-40.6	0.63	-40.6	1	88.4	58.3	0.62	0.88	11,11
9	ok	s=4,m=11	0.34	25.1			1	127.8	84.4	0.90	0.73	11,0
10	NV	s=4,m=11	0.74	-54.6	1.47	-54.6	1	176.7	116.7	1.24	0.50	11,11
11	NV	s=4,m=11	0.74	-54.6	1.47	-54.6	1	176.7	116.7	1.24	0.50	11,11
12	ok	s=4,m=11	0.34	25.1			1	127.8	84.4	0.90	0.73	11,0
13	ok	s=4,m=11	0.55	-40.6	0.63	-40.6	1	88.4	58.3	0.62	0.88	11,11
14	ok	s=4,m=11	0.97	71.2			1	160.0	105.6	1.12	0.58	11,0
15	ok	s=4,m=11	0.52	-38.3	0.59	-38.3	1	88.4	58.3	0.62	0.88	11,11
16	ok	s=4,m=11	0.32	23.7			1	127.8	84.4	0.90	0.73	11,0
17	NV	s=4,m=11	0.70	-51.6	1.39	-51.6	1	176.7	116.7	1.24	0.50	11,11
18	NV	s=4,m=11	0.70	-51.6	1.39	-51.6	1	176.7	116.7	1.24	0.50	11,11
19	ok	s=4,m=11	0.32	23.7			1	127.8	84.4	0.90	0.73	11,0
20	ok	s=4,m=11	0.52	-38.3	0.59	-38.3	1	88.4	58.3	0.62	0.88	11,11
21	ok	s=4,m=11	0.91	67.3			1	160.0	105.6	1.12	0.58	11,0
22	ok	s=4,m=11	0.52	-38.4	0.59	-38.4	1	88.4	58.3	0.62	0.88	11,11
23	ok	s=4,m=11	0.32	23.9			1	127.8	84.4	0.90	0.73	11,0
24	NV	s=4,m=11	0.70	-51.7	1.39	-51.7	1	176.7	116.7	1.24	0.50	11,11
25	NV	s=4,m=11	0.70	-51.7	1.39	-51.7	1	176.7	116.7	1.24	0.50	11,11
26	ok	s=4,m=11	0.32	23.9			1	127.8	84.4	0.90	0.73	11,0
27	ok	s=4,m=11	0.52	-38.4	0.59	-38.4	1	88.4	58.3	0.62	0.88	11,11
28	ok	s=4,m=11	0.92	67.4			1	160.0	105.6	1.12	0.58	11,0
29	ok	s=4,m=11	0.55	-40.4	0.62	-40.4	1	88.4	58.3	0.62	0.88	11,11
30	ok	s=4,m=11	0.34	24.9			1	127.8	84.4	0.90	0.73	11,0
31	NV	s=4,m=11	0.74	-54.3	1.46	-54.3	1	176.7	116.7	1.24	0.50	11,11
32	NV	s=4,m=11	0.74	-54.3	1.46	-54.3	1	176.7	116.7	1.24	0.50	11,11
33	ok	s=4,m=11	0.34	24.9			1	127.8	84.4	0.90	0.73	11,0
34	ok	s=4,m=11	0.55	-40.4	0.62	-40.4	1	88.4	58.3	0.62	0.88	11,11
35	ok	s=4,m=11	0.96	70.8			1	160.0	105.6	1.12	0.58	11,0
Asta			V N	N -54.58	V stab	N -54.58		Beta x L	Snell. LambdaS	Chi mn	v.Omeg	
			0.97	71.24	1.47			176.72	116.65	1.24	0.0	
Trave	Stato	Note	V V/T	V N/M	V stab		Cl.LamS 22LamS 33	Snell.	Chi mn	V flstLamS LT	Chi LT	Rif. cmb
39	NVs=3,m=159		0.20	1.94	0.0		1 3.9	0.8 341.1	0.06	0.55	1.0 0.73	9,11,0,11

INGEGNERE

40	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	9,11,0,11
41	oks=3,m=159	0.02	0.71		1					0.25	0.5	1.00	11,11,0,11
49	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	9,11,0,11
50	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.57	1.2	0.59	9,9,0,11
51	oks=3,m=159	0.03	0.58		1					0.25	0.4	1.00	11,11,0,11
52	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.57	1.2	0.59	9,9,0,11
53	oks=3,m=159	0.03	0.58		1					0.25	0.4	1.00	11,11,0,11
54	NVs=3,m=159	0.20	1.94	0.0	1	3.9	0.8	341.1	0.06	0.55	1.0	0.73	9,11,0,11
55	oks=3,m=159	0.02	0.71		1					0.25	0.5	1.00	11,11,0,11
56	NVs=3,m=159	0.21	3.40	0.0	1	3.9	0.8	341.1	0.06	0.59	1.0	0.73	11,9,0,9
57	NVs=3,m=159	0.24	0.65	0.0	1	3.9	0.4	341.1	0.06	0.57	0.7	0.89	9,9,0,9
58	oks=3,m=159	0.02	0.77		1					0.27	0.5	1.00	9,9,0,9
66	NVs=3,m=159	0.24	0.65	0.0	1	3.9	0.4	341.1	0.06	0.57	0.7	0.89	11,9,0,9
67	NVs=3,m=159	0.21	0.92	0.0	1	3.9	0.8	341.1	0.06	0.60	1.2	0.59	9,9,0,9
68	oks=3,m=159	0.03	0.61		1					0.27	0.4	1.00	9,9,0,9
69	NVs=3,m=159	0.21	0.93	0.0	1	3.9	0.8	341.1	0.06	0.60	1.2	0.59	11,9,0,9
70	oks=3,m=159	0.03	0.61		1					0.27	0.4	1.00	9,9,0,9
71	NVs=3,m=159	0.21	3.40	0.0	1	3.9	0.8	341.1	0.06	0.59	1.0	0.73	9,9,0,9
72	oks=3,m=159	0.02	0.77		1					0.27	0.5	1.00	9,9,0,9
73	NVs=3,m=159	0.20	1.97	0.0	1	3.9	0.8	341.1	0.06	0.55	1.0	0.73	11,9,0,9
74	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	11,9,0,9
75	oks=3,m=159	0.02	0.71		1					0.25	0.5	1.00	9,9,0,9
81	NVs=3,m=159	0.27	0.74		1					1.16	1.2	0.63	11,11,0,11
82	NVs=3,m=159	0.30	1.02		1					1.56	1.2	0.63	11,11,0,11
83	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	11,9,0,9
84	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.57	1.2	0.59	11,11,0,9
85	oks=3,m=159	0.03	0.58		1					0.25	0.4	1.00	9,9,0,9
86	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.57	1.2	0.59	11,11,0,9
87	oks=3,m=159	0.03	0.58		1					0.25	0.4	1.00	9,9,0,9
88	NVs=3,m=159	0.20	1.97	0.0	1	3.9	0.8	341.1	0.06	0.55	1.0	0.73	11,9,0,9
89	oks=3,m=159	0.02	0.71		1					0.25	0.5	1.00	9,9,0,9
90	NVs=3,m=159	0.20	1.96	0.0	1	3.9	0.8	341.1	0.06	0.55	1.0	0.73	11,9,0,9
91	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	9,9,0,9
92	oks=3,m=159	0.02	0.68		1					0.30	1.0	0.82	9,9,0,9
100	NVs=3,m=159	0.23	0.52	0.0	1	3.9	0.4	341.1	0.06	0.54	0.7	0.89	9,9,0,9
101	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.56	1.2	0.59	9,11,0,9
102	oks=3,m=159	0.03	0.54		1					0.25	0.4	1.00	9,9,0,9
103	NVs=3,m=159	0.20	0.68	0.0	1	3.9	0.8	341.1	0.06	0.56	1.2	0.59	9,11,0,9
104	oks=3,m=159	0.03	0.54		1					0.25	0.4	1.00	9,9,0,9
105	NVs=3,m=159	0.20	1.96	0.0	1	3.9	0.8	341.1	0.06	0.55	1.0	0.73	11,9,0,9
106	oks=3,m=159	0.02	0.68		1					0.30	1.0	0.82	9,9,0,9
107	NVs=3,m=159	0.21	3.18	0.0	1	3.9	0.8	341.1	0.06	0.58	1.0	0.73	11,9,0,9
108	NVs=3,m=159	0.24	0.63	0.0	1	3.9	0.4	341.1	0.06	0.57	0.7	0.89	11,9,0,9
109	oks=3,m=159	0.02	0.74		1					0.26	0.5	1.00	9,9,0,9
117	NVs=3,m=159	0.24	0.63	0.0	1	3.9	0.4	341.1	0.06	0.57	0.7	0.89	11,9,0,9
118	NVs=3,m=159	0.21	0.88	0.0	1	3.9	0.8	341.1	0.06	0.60	1.2	0.59	11,9,0,9
119	oks=3,m=159	0.03	0.60		1					0.26	0.4	1.00	9,9,0,9
120	NVs=3,m=159	0.21	0.88	0.0	1	3.9	0.8	341.1	0.06	0.60	1.2	0.59	11,9,0,9
121	oks=3,m=159	0.03	0.60		1					0.26	0.4	1.00	9,9,0,9
122	NVs=3,m=159	0.21	3.18	0.0	1	3.9	0.8	341.1	0.06	0.58	1.0	0.73	11,9,0,9
123	oks=3,m=159	0.02	0.74		1					0.26	0.5	1.00	9,9,0,9
176	NVs=3,m=159	0.32	1.81	3.59	1	4.0	1.2	348.8	0.06	3.31	1.3	0.55	11,11,11,9
179	NVs=3,m=159	0.30	1.05		1					1.70	1.2	0.60	9,9,0,9
180	NVs=3,m=159	0.32	1.10		1					1.76	1.2	0.60	9,9,0,9
181	NVs=6,m=159	0.23	1.01		1					1.00	0.3	1.00	9,11,0,11
182	NVs=6,m=159	0.03	1.00		1					1.00	0.4	1.00	11,11,0,11
183	NVs=6,m=159	0.27	1.09		1					1.09	0.4	1.00	11,11,0,11
184	oks=7,m=159	0.02	0.09		1					0.12	1.0	0.64	3,32,0,32
185	oks=7,m=159	4.64e-03	0.03		1					0.05	1.0	0.64	36,36,0,36
186	oks=7,m=159	0.02	0.07		1					0.11	1.0	0.64	3,31,0,37
187	NVs=7,m=159	0.49	1.17		1					1.86	1.1	0.62	3,3,0,3
188	NVs=7,m=159	0.49	1.16		1					1.86	1.1	0.62	3,3,0,3
189	oks=3,m=159	0.04	0.09		1					0.12	1.0	0.75	9,9,0,9
190	NVs=8,m=159	0.22	1.42		1					1.84	0.9	0.77	4,4,0,3
238	oks=8,m=159	0.09	0.08		1					0.08	0.3	1.00	4,3,0,3
239	oks=8,m=159	0.14	0.52		1					0.57	0.7	0.92	3,3,0,3
240	oks=8,m=159	0.10	0.08		1					0.08	0.3	1.00	3,3,0,3

Trave	V V/T	V N/M	V stab	LamS 22	LamS 33	Snell.	Chi mn	V flst	LamS LT	Chi LT
	0.49	3.40	3.59	4.02	1.16	348.84	0.06	3.31	1.28	0.55

Trave	v.Omeg	f.Om. N	Stato	V N/M	V stab	Rif. cmb	V[7.5.4]	M Ed	V[7.5.5]	N Ed	V[7.5.6]	V Ed,G	V Ed,M
								kN m		kN		kN	kN
39							0.0	0.0	0.0	0.0	0.0	0.0	0.0
40							0.0	0.0	0.0	0.0	0.0	0.0	0.0
41							0.0	0.0	0.0	0.0	0.0	0.0	0.0
49							0.0	0.0	0.0	0.0	0.0	0.0	0.0

INGEGNERE

50	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
51	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
52	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
53	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
54	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
55	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
56	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
57	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
58	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
66	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
67	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
68	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
69	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
70	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
71	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
72	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
73	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
74	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
75	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
81	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
82	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
83	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
84	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
85	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
86	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
87	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
88	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
89	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
90	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
91	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
92	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
101	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
102	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
103	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
104	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
105	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
106	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
107	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
108	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
109	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
117	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
118	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
119	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
120	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
121	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
122	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
123	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
176	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
179	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
180	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
181	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
182	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
183	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
184	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
185	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
186	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
187	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
188	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
189	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
190	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
238	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
239	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
240	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
Trave v.Omeg	V N/M	V stab	V[7.5.4]	M Ed	V[7.5.5]	N Ed	V[7.5.6]	V Ed,G	V Ed,M
			0.0	0.0	0.0	0.0	0.0	0.0	0.0
			0.0	0.0	0.0	0.0	0.0	0.0	0.0

VERIFICHE ELEMENTI MURATURA

LEGENDA TABELLA VERIFICHE ELEMENTI MURATURA

In tabella vengono riportati per ogni elemento il numero dello stesso ed il codice di verifica.

Le verifiche sono state condotte secondo le Norme Tecniche 17 Gennaio 2018.

In particolare sono previste le seguenti verifiche:

Par. 4.5.6.2 Verifiche agli stati limite ultimi, con riferimento in particolare a carichi laterali (fuori dal piano del muro) in assenza di sisma e a stabilità

Par. 7.8.2.2.3 Verifiche a pressoflessione per carichi laterali (fuori dal piano del muro) in presenza di sisma

Par. 7.8.2.2.1 Verifiche a pressoflessione nel piano del muro (in tutte le combinazioni)

Par. 7.8.2.2.2 Verifiche a taglio per azioni nel piano del muro (in tutte le combinazioni)

Par. 7.8.2.2.4 Travi in muratura, con riferimento alle verifiche a flessione e taglio

Con riferimento ai punti succitati le verifiche vengono così tabulate:

Setto/Fascia/Elem.	numero del macroelemento (D3) o elemento (D2) considerato	
Mat.	Materiale	
s=m=	Indice della sezione e del materiale assegnati all' elemento (per D2)	
Spessore	spessore dell'elemento	
Stato	ok L	elemento verificato (stati limite ultimi)
	ok T	elemento verificato (tensioni)
	NV L	elemento non verificato (stati limite ultimi)
	NV T	elemento non verificato (tensioni)

Nodo/Pos.	numero del nodo appartenente al setto / posizione relativa al nodo I per D2
h0/t	valore della snellezza convenzionale
Ecc/t (M)	massimo valore del rapporto $e1/t$ o $e2/t$
Ecc/t	valore del rapporto di eccentricità trasversale utilizzato per la verifica a taglio - Par. 7.8.2.2.2
Fi t	fattore f_i per la riduzione della resistenza in funzione dell'eccentricità trasversale calcolato con Ecc/t
P/A	tensione verticale media (Ao relativamente alla verifica di pressoflessione per carichi laterali in assenza di sisma, Ao(s) relativamente alla verifica di pressoflessione per carichi laterali in presenza di sisma, Ap relativamente alla verifica a pressoflessione nel piano del muro, Av relativamente alla verifica a taglio nel piano del muro per edifici esistenti formula C8.7.1.16 della circolare 21-01-19)
P/Acv	tensione verticale media nella parte compressa, utilizzata nella verifica a taglio nel piano del muro
V. Mo	rapporto tra l' azione assiale di progetto e l' azione assiale ultima in relazione alla verifica Par. 4.5.6.2 (pressoflessione ortogonale) effettuato per le combinazioni senza sisma
V. Mo(S)	rapporto tra l' azione assiale di progetto e l' azione assiale ultima in relazione alla verifica Par. 7.8.2.2.3 (pressoflessione ortogonale) effettuato per le combinazioni con sisma
V. Mp	rapporto tra il momento di progetto e il momento Mrd in relazione alla verifica Par. 7.8.2.2.1 (pressoflessione complanare) effettuato per tutte le combinazioni
Ver. V	rapporto il taglio di progetto e il taglio ultimo in relazione alla verifica Par. 7.8.2.2.2 (taglio complanare) o C8.7.1.16 della circolare 21-01-19 per edifici esistenti effettuato per tutte le combinazioni
	Per travi in muratura:
Ver. V	rapporto tra il taglio di progetto e il minore dei tagli resistenti Vp e Vt in relazione alla verifica del par. 7.8.2.2.3
Rif. cmb	Combinazioni in cui si hanno i massimi valori dei rapporti V. Mo, V. Mo(S), V. Mp, Ver. V

Per elementi consolidati secondo il paragrafo C8.5.3.1 il programma opera come per gli elementi non rinforzati, considerando ai fini delle analisi e delle verifiche gli opportuni coefficienti correttivi delle rigidezze e delle resistenze.

Per elementi consolidati con fibrorinforzi il programma implementa le verifiche previste dalle “Linee guida per la Progettazione, l'Esecuzione ed il Collaudo di Interventi di Rinforzo di strutture di c.a., c.a.p. e murarie mediante FRP” approvate dal CSLP il 24/07/2009. Per questi elementi vengono effettuate le verifiche di resistenza previste al cap. 4.4.1.1.2 flessione ortogonale in assenza/presenza di sisma, 4.4.1.2 flessione e taglio nel piano. Per semplicità la simbologia adottata nelle tabelle è uniformata a quella degli elementi non rinforzati. Le tabelle riportano inoltre i seguenti parametri:

Fibra	Tipo di fibra del fibrorinforzo
E frp	Modulo elastico del fibrorinforzo
epsr	Dilatazione di rottura del fibrorinforzo
epsd	Dilatazione di calcolo
epsd(s)	Dilatazione di calcolo per combinazioni sismiche
Spess.	Spessore del fibrorinforzo, il programma prevede l' applicazione di uno strato di spessore s su entrambe le facce della parete (o sui quattro lati della sezione in caso di confinamento)
AO frp	Area orizzontale complessiva di fibrorinforzo per metro lineare
AV frp	Area verticale complessiva di fibrorinforzo per metro lineare

Affinché l'elemento sia verificato deve essere:

h0/t	non superiore a 20 e al limite imposto per zona sismica e tecnica costruttiva
Ecc/t (M)	non superiore a 0.33
V.Mo, V.Mo(S), V.Mp, Ver.V	non superiore a 1

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
1	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
1	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
2	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
3	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
4	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
5	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
6	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
7	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
8	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
9	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
10	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
11	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
12	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
13	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
14	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
15	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
16	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
17	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
18	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
19	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
20	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
21	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
22	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
23	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
24	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
25	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26

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26	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
27	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
28	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
29	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
30	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
31	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
32	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
33	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
34	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
35	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
36	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26
37	19.4	0.12	0.12	0.32	3.39	2.19	3.27	2.08	1.24	0.06	0.23	0.22 (TC)	11,39,11,26
38	19.4	0.12	0.12	0.32	3.39	2.19	3.39	2.17	1.24	0.06	0.21	0.20 (TC)	11,39,11,26
39	19.4	0.12	0.12	0.32	3.27	1.86	3.27	1.85	1.20	0.17	0.23	0.23 (TC)	11,45,11,26
40	19.4	0.12	0.12	0.31	2.96	1.86	2.96	1.85	1.12	0.17	0.21	0.23 (TC)	11,45,11,26

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	19.43	0.12	0.12	0.31	3.39	2.19	3.39	2.17	1.24	0.17	0.23	0.23

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
2	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
89	19.4	0.12	0.12	0.32	4.54	2.97	4.54	4.54	1.65	0.05	0.16	0.78 (TC)	4,32,4,4
90	19.4	0.12	0.12	0.32	4.91	2.97	4.91	4.91	1.78	0.05	0.51	0.95 (TC)	4,32,4,4
91	19.4	0.12	0.12	0.32	4.91	2.97	4.91	4.91	1.78	0.05	0.51	0.95 (TC)	4,32,4,4
92	19.4	0.12	0.12	0.32	4.54	2.97	4.54	4.54	1.65	0.05	0.16	0.78 (TC)	4,32,4,4
93	19.4	0.12	0.12	0.32	4.91	2.69	4.21	4.21	1.78	0.03	0.59	1.27 (TC)	4,35,4,4
94	19.4	0.12	0.12	0.32	4.91	2.69	4.21	4.21	1.78	0.03	0.59	1.27 (TC)	4,35,4,4
95	19.4	0.12	0.12	0.32	4.21	2.69	4.21	4.21	1.56	0.03	0.59	1.27 (TC)	4,35,4,4
96	19.4	0.12	0.12	0.32	4.21	2.69	4.21	4.21	1.56	0.03	0.59	1.27 (TC)	4,35,4,4
97	19.4	0.12	0.12	0.32	4.91	2.97	4.91	4.91	1.78	0.05	0.51	0.95 (TC)	4,32,4,4
98	19.4	0.12	0.12	0.32	4.54	2.97	4.54	4.54	1.65	0.05	0.16	0.78 (TC)	4,32,4,4
99	19.4	0.12	0.12	0.32	4.91	2.69	4.21	4.21	1.78	0.03	0.59	1.27 (TC)	4,35,4,4
100	19.4	0.12	0.12	0.32	4.21	2.69	4.21	4.21	1.56	0.03	0.59	1.27 (TC)	4,35,4,4

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	19.43	0.12	0.12	0.32	4.91	2.97	4.91	4.91	1.78	0.05	0.59	1.27

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
4	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
41	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.91	1.73	0.08	0.04	0.14 (TC)	11,31,28,29
42	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.98	1.73	0.08	0.04	0.13 (TC)	11,31,28,29
43	19.4	0.12	0.12	0.32	4.68	2.48	4.44	2.91	1.70	0.18	0.04	0.14 (TC)	11,31,4,29
44	19.4	0.12	0.12	0.31	4.04	2.48	3.83	2.48	1.52	0.18	0.03	0.12 (TC)	11,31,4,29
45	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.91	1.73	0.08	0.04	0.14 (TC)	11,31,28,29
46	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.98	1.73	0.08	0.04	0.13 (TC)	11,31,28,29
47	19.4	0.12	0.12	0.32	4.68	2.48	4.44	2.91	1.70	0.18	0.04	0.14 (TC)	11,31,4,29
48	19.4	0.12	0.12	0.31	4.04	2.48	3.83	2.48	1.52	0.18	0.03	0.12 (TC)	11,31,4,29
49	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.91	1.73	0.08	0.04	0.14 (TC)	11,31,28,29
50	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.98	1.73	0.08	0.04	0.13 (TC)	11,31,28,29
51	19.4	0.12	0.12	0.32	4.68	2.48	4.44	2.91	1.70	0.18	0.04	0.14 (TC)	11,31,4,29
52	19.4	0.12	0.12	0.31	4.04	2.48	3.83	2.48	1.52	0.18	0.03	0.12 (TC)	11,31,4,29
53	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.91	1.73	0.08	0.04	0.14 (TC)	11,31,28,29
54	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.98	1.73	0.08	0.04	0.13 (TC)	11,31,28,29
55	19.4	0.12	0.12	0.32	4.68	2.48	4.44	2.91	1.70	0.18	0.04	0.14 (TC)	11,31,4,29
56	19.4	0.12	0.12	0.31	4.04	2.48	3.83	2.48	1.52	0.18	0.03	0.12 (TC)	11,31,4,29
57	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.91	1.73	0.08	0.04	0.14 (TC)	11,31,28,29
58	19.4	0.12	0.12	0.32	4.76	2.99	2.97	2.98	1.73	0.08	0.04	0.13 (TC)	11,31,28,29
59	19.4	0.12	0.12	0.32	4.68	2.48	4.44	2.91	1.70	0.18	0.04	0.14 (TC)	11,31,4,29
60	19.4	0.12	0.12	0.31	4.04	2.48	3.83	2.48	1.52	0.18	0.03	0.12 (TC)	11,31,4,29

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.31								

INGEGNERE

19.43 0.12 0.12 4.76 2.99 4.44 2.98 1.73 0.18 0.04 0.14

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
7	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
61	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
62	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
63	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
64	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
65	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
66	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
67	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
68	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
69	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
70	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
71	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
72	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
73	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
74	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
75	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
76	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
77	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
78	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
79	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
80	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
81	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
82	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
83	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
84	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
85	19.4	0.15	0.14	0.28	5.59	3.55	5.37	3.47	2.37	0.14	0.20	0.20 (TC)	11,41,4,29
86	19.4	0.15	0.14	0.28	5.59	3.55	5.46	3.55	2.37	0.14	0.17	0.19 (TC)	11,41,4,29
87	19.4	0.32	0.14	0.28	5.51	3.08	5.37	3.47	2.32	0.60	0.20	0.20 (TC)	11,34,4,29
88	19.4	0.32	0.0	0.0	0.0	3.08	4.87	3.13	0.0	0.60	0.16	0.18 (TC)	0,34,4,45
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	19.43	0.32	0.14	0.0	5.59	3.55	5.46	3.55	2.37	0.60	0.20	0.20	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
9	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
175	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
176	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
177	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
178	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
179	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
180	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
181	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
182	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
183	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
184	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
185	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
186	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
187	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
188	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
189	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
190	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
191	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
192	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
193	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
194	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
195	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20
196	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
197	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
198	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
199	19.4	0.12	0.11	0.32	3.67	2.46	3.51	2.33	1.33	0.05	0.12	0.23 (TC)	11,34,11,20

200	19.4	0.12	0.11	0.32	3.67	2.46	3.67	2.46	1.33	0.05	0.11	0.19 (TC)	11,34,11,20
201	19.4	0.14	0.12	0.32	3.51	1.95	3.51	1.95	1.29	0.09	0.12	0.31 (TC)	11,33,11,20
202	19.4	0.14	0.13	0.29	2.96	1.95	3.02	1.95	1.19	0.09	0.06	0.31 (TC)	4,33,11,20
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	19.43	0.14	0.13	0.29	3.67	2.46	3.67	2.46	1.33	0.09	0.12	0.31	

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
				daN/cm2	daN/cm2	daN/cm2	daN/cm2						
199	19.4	0.12	0.12	0.31	3.17	2.33	3.17	2.17	1.19	0.03	0.17	1.10 (TC)	4,16,4,34
200	19.4	0.12	0.12	0.32	3.17	2.33	2.31	1.86	1.17	0.03	5.85e-03	1.02 (TC)	4,16,12,34
201	19.4	0.13	0.12	0.31	3.17	1.49	3.17	2.17	1.19	0.04	0.17	1.10 (TC)	4,37,4,34
202	19.4	0.13	0.13	0.30	2.52	1.49	2.47	2.01	1.00	0.04	0.17	0.86 (TC)	4,37,3,34
203	19.4	0.12	0.12	0.31	3.17	2.33	3.17	2.17	1.19	0.03	0.17	1.10 (TC)	4,16,4,34
204	19.4	0.12	0.12	0.32	3.17	2.33	2.31	1.86	1.17	0.03	5.85e-03	1.02 (TC)	4,16,12,34
205	19.4	0.13	0.12	0.31	3.17	1.49	3.17	2.17	1.19	0.04	0.17	1.10 (TC)	4,37,4,34
206	19.4	0.13	0.13	0.30	2.52	1.49	2.47	2.01	1.00	0.04	0.17	0.86 (TC)	4,37,3,34
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	19.43	0.13	0.13	0.30	3.17	2.33	3.17	2.17	1.19	0.04	0.17	1.10	

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/AP	P/ACv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
100	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
202	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
206	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
210	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
214	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
218	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
222	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
226	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
230	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
234	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
238	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
242	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
246	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
251	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
358	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
521	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
527	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
529	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
555	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
558	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
572	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
584	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
612	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
624	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
628	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
651	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
653	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
654	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
657	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
670	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
674	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
678	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
690	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
694	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
702	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
710	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
718	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
722	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
734	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0

INGEGNERE

738	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
742	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
753	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
754	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
755	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
756	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
757	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
758	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
759	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
760	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
761	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
763	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
764	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
765	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
766	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
767	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
768	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
769	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
770	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
771	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
772	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
773	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
775	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
776	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
777	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
779	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
780	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
781	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
783	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
784	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
785	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
786	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
787	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
788	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
789	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
790	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
791	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
792	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
793	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
795	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
796	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
797	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
799	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
800	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
802	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
804	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
812	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
814	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
820	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
830	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
834	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
860	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
888	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
892	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
909	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
910	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
911	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
912	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
916	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
919	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
921	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
925	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
927	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
928	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
929	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
931	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
932	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
956	36.4	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	36.43	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
14	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

INGEGNERE

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
207	19.4	0.16	0.16	0.25	4.28	2.98	3.11	3.01	2.05	0.13	0.15	0.85 (TC)	4,22,36,32
208	19.4	0.15	0.15	0.27	4.43	2.98	3.11	3.12	1.96	0.13	0.15	0.78 (TC)	4,22,36,32
209	19.4	0.23	0.16	0.25	4.28	2.29	2.40	3.01	2.05	0.32	0.11	0.85 (TC)	4,17,34,32
210	19.4	0.23	0.0	0.0	0.0	2.29	2.40	2.42	0.0	0.32	0.11	0.67 (TC)	0,17,34,32
211	19.4	0.16	0.16	0.25	4.28	2.98	3.11	3.01	2.05	0.13	0.15	0.85 (TC)	4,22,36,32
212	19.4	0.15	0.15	0.27	4.43	2.98	3.11	3.12	1.96	0.13	0.15	0.78 (TC)	4,22,36,32
213	19.4	0.23	0.16	0.25	4.28	2.29	2.40	3.01	2.05	0.32	0.11	0.85 (TC)	4,17,34,32
214	19.4	0.23	0.0	0.0	0.0	2.29	2.40	2.42	0.0	0.32	0.11	0.67 (TC)	0,17,34,32
215	19.4	0.16	0.16	0.25	4.28	2.98	3.11	3.01	2.05	0.13	0.15	0.85 (TC)	4,22,36,32
216	19.4	0.15	0.15	0.27	4.43	2.98	3.11	3.12	1.96	0.13	0.15	0.78 (TC)	4,22,36,32
217	19.4	0.23	0.16	0.25	4.28	2.29	2.40	3.01	2.05	0.32	0.11	0.85 (TC)	4,17,34,32
218	19.4	0.23	0.0	0.0	0.0	2.29	2.40	2.42	0.0	0.32	0.11	0.67 (TC)	0,17,34,32

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.0								
	19.43	0.23	0.16		4.43	2.98	3.11	3.12	2.05	0.32	0.15	0.85

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
16	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
219	19.4	0.16	0.16	0.25	4.33	3.01	3.05	2.99	2.07	0.13	0.16	0.78 (TC)	4,30,34,31
220	19.4	0.15	0.15	0.27	4.49	3.01	3.05	3.06	1.98	0.13	0.16	0.72 (TC)	4,30,34,37
221	19.4	0.22	0.16	0.25	4.33	2.34	2.40	2.99	2.07	0.31	0.09	0.78 (TC)	4,30,35,31
222	19.4	0.22	0.0	0.0	0.0	2.34	2.40	2.40	0.0	0.31	0.09	0.63 (TC)	0,30,35,31
223	19.4	0.16	0.16	0.25	4.33	3.01	3.05	2.99	2.07	0.13	0.16	0.78 (TC)	4,30,34,31
224	19.4	0.15	0.15	0.27	4.49	3.01	3.05	3.06	1.98	0.13	0.16	0.72 (TC)	4,30,34,37
225	19.4	0.22	0.16	0.25	4.33	2.34	2.40	2.99	2.07	0.31	0.09	0.78 (TC)	4,30,35,31
226	19.4	0.22	0.0	0.0	0.0	2.34	2.40	2.40	0.0	0.31	0.09	0.63 (TC)	0,30,35,31
227	19.4	0.16	0.16	0.25	4.33	3.01	3.05	2.99	2.07	0.13	0.16	0.78 (TC)	4,30,34,31
228	19.4	0.15	0.15	0.27	4.49	3.01	3.05	3.06	1.98	0.13	0.16	0.72 (TC)	4,30,34,37
229	19.4	0.22	0.16	0.25	4.33	2.34	2.40	2.99	2.07	0.31	0.09	0.78 (TC)	4,30,35,31
230	19.4	0.22	0.0	0.0	0.0	2.34	2.40	2.40	0.0	0.31	0.09	0.63 (TC)	0,30,35,31

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.0								
	19.43	0.22	0.16		4.49	3.01	3.05	3.06	2.07	0.31	0.16	0.78

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
18	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
97	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.29	1.29	0.03	0.18	0.71 (TC)	11,24,38,31
98	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.48	1.29	0.03	0.18	0.64 (TC)	11,24,38,31
99	19.4	0.12	0.12	0.31	3.23	2.25	2.16	2.29	1.23	0.03	0.11	0.71 (TC)	11,33,38,31
100	19.4	0.12	0.12	0.32	2.60	1.84	1.79	1.82	0.96	0.03	0.11	0.59 (TC)	11,28,37,31
231	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.29	1.29	0.03	0.18	0.71 (TC)	11,24,38,31
232	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.48	1.29	0.03	0.18	0.64 (TC)	11,24,38,31
233	19.4	0.12	0.12	0.31	3.23	2.25	2.16	2.29	1.23	0.03	0.11	0.71 (TC)	11,33,38,31
234	19.4	0.12	0.12	0.32	2.60	1.84	1.79	1.82	0.96	0.03	0.11	0.59 (TC)	11,28,37,31
235	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.29	1.29	0.03	0.18	0.71 (TC)	11,24,38,31
236	19.4	0.12	0.12	0.32	3.48	2.48	2.32	2.48	1.29	0.03	0.18	0.64 (TC)	11,24,38,31
237	19.4	0.12	0.12	0.31	3.23	2.25	2.16	2.29	1.23	0.03	0.11	0.71 (TC)	11,33,38,31
238	19.4	0.12	0.12	0.32	2.60	1.84	1.79	1.82	0.96	0.03	0.11	0.59 (TC)	11,28,37,31

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.31								
	19.43	0.12	0.12		3.48	2.48	2.32	2.48	1.29	0.03	0.18	0.71

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
20	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
239	19.4	0.12	0.12	0.32	2.02	1.18	1.17	1.66	0.74	0.01	0.20	1.08 (TC)	11,30,38,31
240	19.4	0.11	0.11	0.32	1.97	1.18	1.19	1.58	0.72	0.01	0.13	1.04 (TC)	11,30,38,31
241	19.4	0.12	0.12	0.32	2.02	1.42	1.82	1.66	0.74	0.02	0.21	1.08 (TC)	11,23,4,31
242	19.4	0.12	0.12	0.32	1.84	1.42	1.82	1.52	0.67	0.02	0.21	0.95 (TC)	11,23,4,31
243	19.4	0.12	0.12	0.32	2.02	1.18	1.17	1.66	0.74	0.01	0.20	1.08 (TC)	11,30,38,31
244	19.4	0.11	0.11	0.32	1.97	1.18	1.19	1.58	0.72	0.01	0.13	1.04 (TC)	11,30,38,31
245	19.4	0.12	0.12	0.32	2.02	1.42	1.82	1.66	0.74	0.02	0.21	1.08 (TC)	11,23,4,31
246	19.4	0.12	0.12	0.32	1.84	1.42	1.82	1.52	0.67	0.02	0.21	0.95 (TC)	11,23,4,31
355	19.4	0.11	0.11	0.32	1.97	1.18	1.19	1.58	0.72	0.01	0.13	1.04 (TC)	11,30,38,31
356	19.4	0.12	0.12	0.32	2.02	1.18	1.17	1.66	0.74	0.01	0.20	1.08 (TC)	11,30,38,31
357	19.4	0.12	0.12	0.32	2.02	1.42	1.82	1.66	0.74	0.02	0.21	1.08 (TC)	11,23,4,31
358	19.4	0.12	0.12	0.32	1.84	1.42	1.82	1.52	0.67	0.02	0.21	0.95 (TC)	11,23,4,31

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.32								
	19.43	0.12	0.12		2.02	1.42	1.82	1.66	0.74	0.02	0.21	1.08

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
22	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	25.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
249	10.9	0.07	0.07	0.64	2.06	1.49	1.79	1.15	0.38	0.02	0.06	0.33 (TC)	11,30,3,44
250	10.9	0.07	0.07	0.64	2.06	1.49	2.02	1.82	0.38	0.02	0.01	0.25 (TC)	11,30,9,45
252	10.9	0.07	0.07	0.63	1.85	0.97	1.79	0.92	0.34	0.02	0.06	0.46 (TC)	11,46,3,44
254	10.9	0.07	0.07	0.62	1.27	0.97	1.23	0.92	0.24	0.02	0.04	0.46 (TC)	11,46,3,44
255	10.9	0.07	0.07	0.64	2.06	1.49	1.79	1.15	0.38	0.02	0.06	0.33 (TC)	11,30,3,44
256	10.9	0.07	0.07	0.64	2.06	1.49	2.02	1.82	0.38	0.02	0.01	0.25 (TC)	11,30,9,45
257	10.9	0.07	0.07	0.63	1.85	0.97	1.79	0.92	0.34	0.02	0.06	0.46 (TC)	11,46,3,44
258	10.9	0.07	0.07	0.62	1.27	0.97	1.23	0.92	0.24	0.02	0.04	0.46 (TC)	11,46,3,44

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
				0.62								
	10.88	0.07	0.07		2.06	1.49	2.02	1.82	0.38	0.02	0.06	0.46

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
23	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
7	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
8	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
12	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
16	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
20	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
24	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
28	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
32	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
36	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
40	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
44	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
48	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
52	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
56	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
60	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
64	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
68	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
72	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
76	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
80	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
84	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
88	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
95	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
96	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25
102	18.2	0.27	0.0	0.0	0.0	1.13	1.54	1.14	0.0	0.59	0.02	0.11 (TC)	0,35,12,25

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t 0.0	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	18.21	0.27	0.15		1.68	1.13	1.54	1.14	0.68	0.59	0.05	0.12

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
25	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	25.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
243	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
244	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
245	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
246	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
259	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
260	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
261	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
262	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
263	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
264	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
265	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
266	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
267	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
268	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
269	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
270	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
271	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
272	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
273	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
274	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
275	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
276	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
277	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
278	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
279	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
280	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
281	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
282	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
283	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
284	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
285	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
286	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
287	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
288	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
289	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
290	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
291	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
292	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
293	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
294	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
295	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
296	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
297	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
298	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
299	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
300	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
301	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
302	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
303	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
304	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
305	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
306	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
307	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
308	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
309	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
310	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
311	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
312	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
313	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
314	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
315	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
316	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
317	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
318	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
319	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
320	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
321	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
322	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27

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323	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
324	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
325	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
326	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
327	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
328	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
329	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
330	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
331	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
332	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
333	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
334	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
335	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
336	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
337	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
338	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
339	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
340	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
341	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
342	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
343	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
344	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
345	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
346	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
347	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
348	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
349	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
350	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
351	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
352	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
353	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
354	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27
379	10.9	0.07	0.07	0.64	1.97	1.33	1.23	1.27	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
380	10.9	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.15	0.04	0.15 (TC)	11,36,38,27
381	10.9	0.07	0.06	0.64	1.83	1.06	1.23	1.05	0.33	0.21	0.04	0.16 (TC)	11,45,38,27
382	10.9	0.07	0.07	0.64	1.56	1.06	1.04	1.05	0.29	0.21	0.04	0.16 (TC)	11,45,38,27

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	10.88	0.07	0.07	0.64	1.97	1.33	1.33	1.37	0.36	0.21	0.04	0.16

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
26	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
355	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
356	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
357	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
358	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
359	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
360	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
361	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
362	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
363	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
364	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
365	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
366	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
367	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
368	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
369	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
370	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
371	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
372	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
373	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
374	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
375	19.4	0.12	0.11	0.32	1.86	1.15	1.07	1.16	0.68	0.09	0.12	0.17 (TC)	4,37,23,26
376	19.4	0.11	0.11	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.16 (TC)	4,37,23,26
377	19.4	0.12	0.12	0.32	1.72	0.80	1.07	0.84	0.63	0.08	0.12	0.18 (TC)	4,37,23,26
378	19.4	0.12	0.12	0.32	1.32	0.80	0.80	0.84	0.48	0.08	0.11	0.18 (TC)	4,37,35,26
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	19.43	0.12	0.12	0.32	1.86	1.15	1.17	1.29	0.68	0.09	0.12	0.18	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
28	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
414	12.3	0.17	0.17	0.38	1.04	0.71	1.04	0.74	0.32	0.51	0.02	0.38 (TC)	11,30,9,41
418	12.3	0.17	0.17	0.38	1.04	0.71	1.04	0.74	0.32	0.51	0.02	0.38 (TC)	11,30,9,41
652	12.3	0.12	0.12	0.48	0.68	0.43	0.53	0.43	0.17	0.54	0.07	0.14 (TC)	11,29,12,39
864	12.3	0.12	0.12	0.48	0.68	0.43	0.53	0.43	0.17	0.54	0.07	0.14 (TC)	11,29,12,39
918	12.3	0.16	0.16	0.41	0.84	0.56	0.53	0.57	0.24	0.72	0.07	0.23 (TC)	11,30,12,45
965	12.3	0.21	0.21	0.31	1.09	0.74	1.04	0.74	0.41	0.68	0.02	0.38 (TC)	9,30,9,41
967	12.3	0.21	0.21	0.31	1.09	0.56	0.66	0.77	0.41	0.72	0.02	0.32 (TC)	9,30,12,41
969	12.3	0.21	0.21	0.31	1.09	0.74	1.04	0.74	0.41	0.68	0.02	0.38 (TC)	9,30,9,41
971	12.3	0.21	0.21	0.31	1.09	0.56	0.66	0.77	0.41	0.72	0.02	0.32 (TC)	9,30,12,41
972	12.3	0.16	0.16	0.41	0.84	0.56	0.53	0.57	0.24	0.72	0.07	0.23 (TC)	11,30,12,45
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	12.35	0.21	0.21	0.31	1.09	0.74	1.04	0.77	0.41	0.72	0.07	0.38	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
30	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
178	18.2	0.40	0.0	0.0	0.0	0.40	0.39	0.41	0.0	0.47	0.54	1.35 (TC)	0,33,7,31
253	18.2	0.40	0.0	0.0	0.0	0.40	0.39	0.40	0.0	0.47	0.54	1.95 (TC)	0,33,7,3
553	18.2	0.40	0.0	0.0	0.0	0.40	0.39	0.41	0.0	0.47	0.54	1.35 (TC)	0,33,7,31
564	18.2	0.28	0.13	0.32	0.35	0.29	0.28	0.40	0.13	0.27	0.35	1.95 (TC)	11,31,12,3
568	18.2	0.15	0.13	0.32	0.35	0.16	0.28	0.27	0.13	0.12	0.35	1.00 (TC)	11,31,12,34
729	18.2	0.40	0.0	0.0	0.0	0.40	0.39	0.40	0.0	0.47	0.54	1.95 (TC)	0,33,7,3
731	18.2	0.28	0.13	0.32	0.35	0.29	0.28	0.40	0.13	0.27	0.35	1.95 (TC)	11,31,12,3
732	18.2	0.15	0.13	0.32	0.35	0.16	0.28	0.27	0.13	0.12	0.35	1.00 (TC)	11,31,12,34
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	18.21	0.40	0.13	0.0	0.35	0.40	0.39	0.41	0.13	0.47	0.54	1.95	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
33	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
451	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
452	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
453	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
455	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
456	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
457	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
459	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
460	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
461	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
463	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
464	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
465	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
467	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
468	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
469	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
471	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
472	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
473	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
475	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.78	0.40	0.37	0.22	0.14 (TC)	11,19,43,40
476	9.7	0.20	0.19	0.40	1.16	0.84	0.77	0.78	0.34	0.29	0.21	0.14 (TC)	9,22,39,40
477	9.7	0.24	0.24	0.30	1.03	0.65	0.68	0.69	0.40	0.37	0.22	0.14 (TC)	11,19,43,40

INGEGNERE

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	9.71	0.24	0.24	0.30	1.16	0.84	0.77	0.78	0.40	0.37	0.22	0.14

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
35	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
479	9.7	0.07	0.07	0.66	0.91	0.40	0.46	0.85	0.16	0.11	0.26	0.36 (TC)	11,20,20,11
480	9.7	0.07	0.07	0.67	0.85	0.40	0.40	0.85	0.15	0.11	0.07	0.36 (TC)	9,20,20,11
481	9.7	0.07	0.07	0.66	0.91	0.46	0.46	0.52	0.16	0.05	0.26	0.34 (TC)	11,20,20,27
483	9.7	0.07	0.07	0.66	0.91	0.40	0.46	0.85	0.16	0.11	0.26	0.36 (TC)	11,20,20,11
484	9.7	0.07	0.07	0.67	0.85	0.40	0.40	0.85	0.15	0.11	0.07	0.36 (TC)	9,20,20,11
485	9.7	0.07	0.07	0.66	0.91	0.46	0.46	0.52	0.16	0.05	0.26	0.34 (TC)	11,20,20,27
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	9.71	0.07	0.07	0.66	0.91	0.46	0.46	0.85	0.16	0.11	0.26	0.36	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
37	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
525	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
526	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
528	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
529	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
530	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
531	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
532	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
533	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
534	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
535	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
536	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
537	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
538	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
539	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
540	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
541	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
542	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
543	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
544	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
545	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
546	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
547	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
548	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
549	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
550	19.4	0.13	0.12	0.31	1.84	1.13	1.12	1.19	0.69	0.18	0.23	0.14 (TC)	9,37,15,21
551	19.4	0.12	0.12	0.31	1.84	1.13	1.24	1.30	0.69	0.18	0.22	0.13 (TC)	9,37,15,17
552	19.4	0.14	0.13	0.29	1.66	1.01	1.12	0.95	0.66	0.15	0.23	0.14 (TC)	11,37,15,21
553	19.4	0.14	0.14	0.29	1.35	1.15	0.90	0.95	0.55	0.12	0.21	0.14 (TC)	11,34,15,21
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	19.43	0.14	0.14	0.29	1.84	1.15	1.24	1.30	0.69	0.18	0.23	0.14	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
41	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
182	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15

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186	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15
190	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15
194	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15
198	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15
202	18.2	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.22	0.22 (TC)	11,32,11,15
733	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
735	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
736	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15
737	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
739	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
740	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15
741	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
743	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
744	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15
745	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
747	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
748	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15
749	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
751	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
752	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15
753	18.2	0.14	0.14	0.31	1.83	1.14	1.48	0.89	0.70	0.25	0.24	0.22 (TC)	11,32,9,15
755	18.2	0.12	0.12	0.35	1.48	0.89	0.90	0.89	0.50	0.20	0.25	0.22 (TC)	11,32,9,15
756	18.2	0.11	0.11	0.36	0.90	0.52	0.90	0.52	0.29	0.16	0.25	0.19 (TC)	11,32,9,15

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	18.21	0.14	0.14	0.31	1.83	1.14	1.83	1.12	0.70	0.25	0.25	0.22

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
45	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	25.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
258	8.5	0.06	0.06	0.70	0.40	0.24	0.38	0.20	0.07	0.06	0.07	0.29 (TC)	11,29,3,45
262	8.5	0.06	0.06	0.70	0.40	0.24	0.38	0.20	0.07	0.06	0.07	0.29 (TC)	11,29,3,45
640	8.5	0.08	0.08	0.66	0.26	0.20	0.20	0.16	0.05	0.12	0.14	0.28 (TC)	11,42,14,41
809	8.5	0.06	0.06	0.70	0.40	0.24	0.38	0.20	0.07	0.06	0.07	0.29 (TC)	11,29,3,45
811	8.5	0.08	0.06	0.70	0.38	0.20	0.20	0.16	0.06	0.12	0.14	0.28 (TC)	11,42,14,41
813	8.5	0.06	0.06	0.70	0.40	0.24	0.38	0.20	0.07	0.06	0.07	0.29 (TC)	11,29,3,45
815	8.5	0.08	0.06	0.70	0.38	0.20	0.20	0.16	0.06	0.12	0.14	0.28 (TC)	11,42,14,41

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	8.52	0.08	0.08	0.66	0.40	0.24	0.38	0.20	0.07	0.12	0.14	0.29

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
46	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
390	12.3	0.17	0.17	0.38	0.95	0.65	0.95	0.67	0.29	0.53	0.01	0.42 (TC)	9,21,11,40
394	12.3	0.17	0.17	0.38	0.95	0.65	0.95	0.67	0.29	0.53	0.01	0.42 (TC)	9,21,11,40
816	12.3	0.17	0.17	0.39	0.80	0.53	0.49	0.56	0.24	0.74	0.09	0.24 (TC)	9,21,14,42
828	12.3	0.13	0.13	0.45	0.62	0.39	0.49	0.40	0.16	0.60	0.09	0.15 (TC)	9,22,14,40
832	12.3	0.17	0.17	0.39	0.80	0.53	0.49	0.56	0.24	0.74	0.09	0.24 (TC)	9,21,14,42
923	12.3	0.13	0.13	0.45	0.62	0.39	0.49	0.40	0.16	0.60	0.09	0.15 (TC)	9,22,14,40
941	12.3	0.21	0.21	0.31	1.05	0.71	1.05	0.67	0.40	0.69	0.02	0.42 (TC)	9,21,9,40
943	12.3	0.21	0.21	0.31	1.05	0.53	0.63	0.73	0.40	0.74	0.04	0.32 (TC)	9,21,12,40
945	12.3	0.21	0.21	0.31	1.05	0.71	1.05	0.67	0.40	0.69	0.02	0.42 (TC)	9,21,9,40
947	12.3	0.21	0.21	0.31	1.05	0.53	0.63	0.73	0.40	0.74	0.04	0.32 (TC)	9,21,12,40

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	12.35	0.21	0.21	0.31	1.05	0.71	1.05	0.73	0.40	0.74	0.09	0.42

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
47	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	25.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/AP	P/ACv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
262	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
266	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
270	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
274	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
278	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
282	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
286	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
290	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
294	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
298	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
302	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
306	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
310	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
314	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
318	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
322	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
326	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
330	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
334	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
338	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
342	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
346	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
350	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
382	8.7	0.06	0.05	0.72	0.74	0.48	0.74	0.48	0.12	0.67	0.08	0.05 (TC)	11,37,11,27
813	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
815	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
817	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
819	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
821	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
823	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
825	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
827	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
829	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
831	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
833	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
835	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
837	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
839	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
841	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
843	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
845	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
847	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
849	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
851	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
853	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
855	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
857	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
859	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
861	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
863	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
865	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
867	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
869	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
871	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
873	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
875	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
877	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
879	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
881	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
883	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
885	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
887	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
889	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
891	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23
893	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
895	8.7	0.06	0.06	0.72	0.61	0.38	0.48	0.28	0.10	0.53	0.17	0.05 (TC)	9,44,11,23
897	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
899	8.7	0.06	0.06	0.72	0.61	0.38	0.48	0.28	0.10	0.53	0.17	0.05 (TC)	9,44,11,23
900	8.7	0.06	0.06	0.69	0.48	0.28	0.48	0.28	0.08	0.32	0.17	0.05 (TC)	11,44,11,23
901	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
903	8.7	0.06	0.06	0.72	0.61	0.38	0.48	0.28	0.10	0.53	0.17	0.05 (TC)	9,44,11,23
904	8.7	0.06	0.06	0.69	0.48	0.28	0.48	0.28	0.08	0.32	0.17	0.05 (TC)	11,44,11,23
933	8.7	0.06	0.05	0.72	0.74	0.48	0.61	0.48	0.12	0.67	0.10	0.05 (TC)	11,37,11,27
935	8.7	0.06	0.06	0.72	0.61	0.38	0.61	0.38	0.10	0.53	0.10	0.05 (TC)	9,44,11,23

INGEGNERE

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	8.74	0.06	0.06	0.69	0.74	0.48	0.74	0.48	0.12	0.67	0.17	0.05

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
50	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	25.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
246	10.2	0.07	0.07	0.65	0.79	0.54	0.56	0.53	0.14	0.10	0.03	0.33 (TC)	11,35,7,37
354	10.2	0.07	0.07	0.65	0.79	0.54	0.56	0.53	0.14	0.10	0.03	0.33 (TC)	11,35,7,37
797	10.2	0.07	0.07	0.65	0.79	0.54	0.56	0.53	0.14	0.10	0.03	0.33 (TC)	11,35,7,37
799	10.2	0.07	0.07	0.66	0.71	0.28	0.33	0.71	0.13	0.13	0.24	0.29 (TC)	11,36,14,11
800	10.2	0.06	0.06	0.67	0.43	0.28	0.33	0.43	0.08	0.13	0.24	0.21 (TC)	11,36,14,11
905	10.2	0.07	0.07	0.65	0.79	0.54	0.56	0.53	0.14	0.10	0.03	0.33 (TC)	11,35,7,37
907	10.2	0.07	0.07	0.66	0.71	0.28	0.33	0.71	0.13	0.13	0.24	0.29 (TC)	11,36,14,11
908	10.2	0.06	0.06	0.67	0.43	0.28	0.33	0.43	0.08	0.13	0.24	0.21 (TC)	11,36,14,11

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	10.20	0.07	0.07	0.65	0.79	0.54	0.56	0.71	0.14	0.13	0.24	0.33

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
51	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	ok L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
253	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
522	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
529	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
533	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
537	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
541	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
545	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
549	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
553	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
564	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
568	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
909	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
916	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
919	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
924	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
930	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
934	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
938	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
942	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
944	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
946	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
950	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
952	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
954	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
958	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17
962	18.2	0.11	0.11	0.36	0.43	0.25	0.25	0.27	0.14	0.11	0.05	0.07 (TC)	11,37,31,15
966	18.2	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13 (TC)	9,31,31,17
970	18.2	0.11	0.11	0.36	0.72	0.43	0.46	0.49	0.24	0.24	0.09	0.11 (TC)	11,39,15,17

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	18.21	0.11	0.11	0.36	0.92	0.54	0.54	0.63	0.30	0.28	0.16	0.13

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
52	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
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Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
54	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

[illegible]

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
55	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04-muratura E = 1.500e+04	14.0	4.05	3.24	NV L

[illegible]

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
56	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	25.0	4.05	3.24	NV L

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
57	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	14.0	4.05	3.24	NV L

[illegible]

INGEGNERE

512	25.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
513	25.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0
514	25.9	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0 (nd)	0,0,0,0

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	25.90	0.0	0.0	0.0									
				0.0									
					0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
59	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
483	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
484	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
485	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
486	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
487	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
488	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
489	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
490	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
491	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
492	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
493	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
494	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
495	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
496	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
497	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
498	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
499	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
500	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
501	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
502	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
503	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
504	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
505	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
506	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20
507	11.9	0.24	0.24	0.25	1.16	0.83	0.63	0.63	0.54	0.36	0.23	0.22 (TC)	11,39,20,20
508	11.9	0.24	0.24	0.25	1.16	0.83	0.75	0.75	0.54	0.36	0.19	0.20 (TC)	11,39,20,20
509	11.9	0.73	0.18	0.37	0.99	0.43	0.42	0.42	0.31	1.30	0.27	0.26 (TC)	11,19,20,20
510	11.9	0.73	0.0	0.0	0.0	0.43	0.42	0.42	0.0	1.30	0.27	0.26 (TC)	0,19,20,20

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	11.91	0.73	0.24	0.0									
				0.0									
					1.16	0.83	0.75	0.75	0.54	1.30	0.27	0.26	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
		cm			
63	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	28.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
435	11.1	0.21	0.21	0.34	1.10	0.82	0.61	0.82	0.38	0.29	0.24	0.28 (TC)	9,44,19,22
436	11.1	0.21	0.21	0.34	1.10	0.82	0.74	0.82	0.38	0.29	0.23	0.28 (TC)	9,44,19,22
437	11.1	0.70	0.19	0.38	0.97	0.38	0.39	0.51	0.30	1.33	0.24	0.28 (TC)	9,15,43,22
438	11.1	0.70	0.0	0.0	0.0	0.38	0.39	0.51	0.0	1.33	0.24	0.28 (TC)	0,15,43,22
439	11.1	0.21	0.21	0.34	1.10	0.82	0.61	0.82	0.38	0.29	0.24	0.28 (TC)	9,44,19,22
440	11.1	0.21	0.21	0.34	1.10	0.82	0.74	0.82	0.38	0.29	0.23	0.28 (TC)	9,44,19,22
441	11.1	0.70	0.19	0.38	0.97	0.38	0.39	0.51	0.30	1.33	0.24	0.28 (TC)	9,15,43,22
442	11.1	0.70	0.0	0.0	0.0	0.38	0.39	0.51	0.0	1.33	0.24	0.28 (TC)	0,15,43,22
443	11.1	0.21	0.21	0.34	1.10	0.82	0.61	0.82	0.38	0.29	0.24	0.28 (TC)	9,44,19,22
444	11.1	0.21	0.21	0.34	1.10	0.82	0.74	0.82	0.38	0.29	0.23	0.28 (TC)	9,44,19,22
445	11.1	0.70	0.19	0.38	0.97	0.38	0.39	0.51	0.30	1.33	0.24	0.28 (TC)	9,15,43,22
446	11.1	0.70	0.0	0.0	0.0	0.38	0.39	0.51	0.0	1.33	0.24	0.28 (TC)	0,15,43,22
447	11.1	0.21	0.21	0.34	1.10	0.82	0.61	0.82	0.38	0.29	0.24	0.28 (TC)	9,44,19,22
448	11.1	0.21	0.21	0.34	1.10	0.82	0.74	0.82	0.38	0.29	0.23	0.28 (TC)	9,44,19,22
449	11.1	0.70	0.19	0.38	0.97	0.38	0.39	0.51	0.30	1.33	0.24	0.28 (TC)	9,15,43,22
450	11.1	0.70	0.0	0.0	0.0	0.38	0.39	0.51	0.0	1.33	0.24	0.28 (TC)	0,15,43,22
451	11.1	0.21	0.21	0.34	1.10	0.82	0.61	0.82	0.38	0.29	0.24	0.28 (TC)	9,44,19,22
452	11.1	0.21	0.21	0.34	1.10	0.82	0.74	0.82	0.38	0.29	0.23	0.28 (TC)	9,44,19,22
453	11.1	0.70	0.19	0.38	0.97	0.38	0.39	0.51	0.30	1.33	0.24	0.28 (TC)	9,15,43,22

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454	11.1	0.70	0.0	0.0	0.0	0.38	0.39	0.51	0.0	1.33	0.24	0.28 (TC)	0,15,43,22
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	11.12	0.70	0.21	0.0	1.10	0.82	0.74	0.82	0.38	1.33	0.24	0.28	

Setto	Mat.	Spessore	Gamma non sis.	Gamma sis.	Stato
65	Muratura in mattoni pieni e malta di calce - Circ. n7/2019-muratura E = 1.500e+04- muratura E = 1.500e+04	cm 28.0	4.05	3.24	NV L

Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
					daN/cm2	daN/cm2	daN/cm2	daN/cm2					
387	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.18	0.55	0.22	0.13	0.23 (TC)	9,40,19,19
388	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.25	0.55	0.22	0.13	0.22 (TC)	9,40,19,19
389	13.0	0.29	0.25	0.21	0.84	0.88	1.18	1.18	0.46	0.42	0.11	0.23 (TC)	7,40,19,19
390	13.0	0.29	0.25	0.21	0.84	0.88	0.87	0.84	0.46	0.42	0.11	0.21 (TC)	7,40,42,22
423	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.18	0.55	0.22	0.13	0.23 (TC)	9,40,19,19
424	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.25	0.55	0.22	0.13	0.22 (TC)	9,40,19,19
425	13.0	0.29	0.25	0.21	0.84	0.88	1.18	1.18	0.46	0.42	0.11	0.23 (TC)	7,40,19,19
426	13.0	0.29	0.25	0.21	0.84	0.88	0.87	0.84	0.46	0.42	0.11	0.21 (TC)	7,40,42,22
427	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.18	0.55	0.22	0.13	0.23 (TC)	9,40,19,19
428	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.25	0.55	0.22	0.13	0.22 (TC)	9,40,19,19
429	13.0	0.29	0.25	0.21	0.84	0.88	1.18	1.18	0.46	0.42	0.11	0.23 (TC)	7,40,19,19
430	13.0	0.29	0.25	0.21	0.84	0.88	0.87	0.84	0.46	0.42	0.11	0.21 (TC)	7,40,42,22
431	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.18	0.55	0.22	0.13	0.23 (TC)	9,40,19,19
432	13.0	0.17	0.16	0.38	1.77	1.27	1.25	1.25	0.55	0.22	0.13	0.22 (TC)	9,40,19,19
433	13.0	0.29	0.25	0.21	0.84	0.88	1.18	1.18	0.46	0.42	0.11	0.23 (TC)	7,40,19,19
434	13.0	0.29	0.25	0.21	0.84	0.88	0.87	0.84	0.46	0.42	0.11	0.21 (TC)	7,40,42,22
Nodo	h0/t	Ecc/t(M)	Ecc/t	Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	
	12.95	0.29	0.25	0.21	1.77	1.27	1.25	1.25	0.55	0.42	0.13	0.23	

TABELLA VERIFICHE ELEMENTI D2 MASCHI MURATURA

Elem.	Note	Pos.	h0/t Ecc/t(M)		Fi t	P/Ao	P/Ao(s)	P/Ap	P/Acv	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V	Rif. cmb
daN/cm2daN/cm2daN/cm2daN/cm2														
36	ok L	0.0	1.8	0.02	0.94	0.99	0.74	0.77	0.99	0.12	0.03	0.025.10e-03 (TC)	9,42,12,11	
	s=1,m=108	106.7	1.8	0.01	0.95	0.74	0.54	0.53	0.74	0.09	0.01	0.025.66e-03 (TC)	9,40,21,11	
37	NV L	0.0	1.8	0.02	0.93	1.54	1.04	1.03	1.03	0.19	0.03	0.95 0.07 (TC)	11,45,30,25	
	s=1,m=108	106.7	1.8	0.01	0.95	1.29	0.83	0.84	0.83	0.16	0.01	1.31 0.08 (TC)	11,21,30,25	
38	NV L	0.0	1.8	0.02	0.93	1.53	1.05	1.02	1.02	0.19	0.03	0.93 0.08 (TC)	9,40,21,22	
	s=1,m=108	106.7	1.8	0.02	0.93	1.28	0.83	0.83	0.83	0.16	0.03	1.32 0.09 (TC)	9,29,21,22	
42	NV L	0.0	7.2	0.06	0.73	5.16	3.15	5.16	5.16	0.83	0.17	2.67 0.80 (TC)	3,36,3,4	
	s=2,m=108	320.0	7.2	0.09	0.66	4.41	2.58	4.41	4.41	0.79	0.26	4.76 0.86 (TC)	3,36,4,4	
43	NV L	0.0	7.2	0.06	0.75	5.11	3.14	5.11	5.11	0.80	0.16	2.62 0.80 (TC)	4,37,4,4	
	s=2,m=108	320.0	7.2	0.08	0.68	4.36	2.56	4.36	4.36	0.75	0.23	4.72 0.86 (TC)	4,37,4,4	
44	ok L	0.0	1.8	0.03	0.90	3.66	2.36	2.34	2.34	0.48	0.40	0.07 0.05 (TC)	11,43,26,26	
	s=1,m=108	106.7	1.8	0.01	0.95	3.41	2.17	3.41	2.15	0.42	0.10	0.01 0.05 (TC)	11,45,11,26	
45	ok L	0.0	1.8	0.02	0.92	4.38	2.79	2.73	2.73	0.56	0.44	0.08 0.05 (TC)	11,43,26,26	
	s=1,m=108	106.7	1.8	0.01	0.95	4.13	2.58	4.13	2.54	0.51	0.10	0.02 0.05 (TC)	11,45,11,26	
46	ok L	0.0	1.8	0.03	0.91	4.67	2.96	2.96	2.96	0.60	0.40	0.06 0.04 (TC)	11,31,29,29	
	s=1,m=108	106.7	1.8	0.01	0.95	4.42	2.77	2.77	2.77	0.55	0.104.44e-03	0.04 (TC)	11,33,29,29	
47	NV L	0.0	1.8	0.28	0.39	4.69	3.36	3.36	3.36	1.43	0.89	0.06 0.04 (TC)	3,33,29,29	
	s=1,m=108	106.7	1.8	0.02	0.94	4.98	3.06	4.44	3.17	0.62	0.116.81e-03	0.04 (TC)	11,32,3,29	
48	ok L	0.0	1.8	0.03	0.92	6.24	4.02	6.24	3.87	0.80	0.22	0.17 0.05 (TC)	11,36,11,29	
	s=1,m=108	106.7	1.8	0.01	0.95	5.99	3.82	5.99	3.67	0.74	0.077.80e-03	0.05 (TC)	11,32,11,29	
59	ok L	0.0	1.8	0.02	0.93	3.86	2.61	3.86	3.86	0.49	0.24	0.24 0.15 (TC)	11,31,4,4	
	s=1,m=108	106.7	1.8	0.01	0.95	3.61	2.49	3.61	3.61	0.45	0.02	0.07 0.16 (TC)	4,38,4,4	
60	NV L	0.0	1.8	0.02	0.95	4.60	3.20	4.60	4.50	0.57	0.23	1.31 0.59 (TC)	4,31,4,3	
	s=1,m=108	106.7	1.8	0.01	0.95	4.35	2.93	3.00	4.26	0.548.72e-03	0.05	0.60 (TC)	4,38,27,3	
61	NV L	0.0	1.8	0.02	0.92	4.55	3.22	4.55	4.46	0.58	0.26	1.29 0.59 (TC)	4,32,4,3	
	s=1,m=108	106.7	1.8	0.01	0.95	4.30	2.85	2.96	4.21	0.539.29e-03	0.05	0.60 (TC)	4,33,19,3	
62	ok L	0.0	1.8	0.04	0.88	3.38	2.86	2.10	2.10	0.45	0.27	0.07 0.03 (TC)	4,32,21,21	
	s=1,m=108	106.7	1.8	0.02	0.94	3.13	1.73	1.73	1.91	0.39	0.07	0.02 0.03 (TC)	4,33,33,21	
63	ok L	0.0	1.8	0.04	0.88	4.15	2.71	2.63	2.63	0.55	0.26	0.06 0.04 (TC)	11,31,20,20	
	s=1,m=108	106.7	1.8	0.01	0.96	3.90	2.46	2.51	2.44	0.48	0.095.32e-03	0.04 (TC)	11,38,31,20	
64	NV L	0.0	1.8	0.32	0.35	3.25	2.19	2.28	2.28	1.09	1.00	0.08 0.05 (TC)	4,34,21,21	
	s=1,m=108	106.7	1.8	0.05	0.90	3.16	2.12	2.09	2.09	0.41	0.28	0.01 0.05 (TC)	11,31,21,21	
65	ok L	0.0	1.8	0.08	0.73	2.90	1.87	1.87	1.91	0.46	0.80	0.04 0.03 (TC)	9,32,20,21	

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s=1,m=108	106.7	1.8	0.08	0.74	2.65	1.68	1.72	1.72	0.42	0.747.19e-03	0.03 (TC)	9,32,17,21	
76 ok L	0.0	1.8	0.10	0.70	2.86	1.85	1.84	1.84	0.48	0.92	0.05	0.03 (TC)	11,40,20,20
s=1,m=108	106.7	1.8	0.09	0.71	2.62	1.65	1.69	1.65	0.43	0.844.74e-03	0.03 (TC)	11,40,21,20	
77 ok L	0.0	1.8	0.10	0.71	2.75	1.82	1.80	1.81	0.46	0.78	0.04	0.02 (TC)	9,42,20,21
s=1,m=108	106.7	1.8	0.09	0.72	2.50	1.63	1.62	1.62	0.41	0.726.18e-03	0.02 (TC)	9,42,21,21	
78 ok L	0.0	1.8	0.04	0.86	2.00	1.57	1.30	1.50	0.27	0.14	0.04	0.02 (TC)	9,40,19,21
s=1,m=108	106.7	1.8	0.02	0.94	1.75	1.07	1.11	1.30	0.22	0.03	0.01	0.02 (TC)	9,39,19,21
79 ok L	0.0	1.8	0.01	0.95	2.63	1.80	1.80	2.63	0.33	0.09	0.42	0.15 (TC)	11,40,22,9
s=1,m=108	106.7	1.8	0.01	0.95	2.38	1.73	1.61	2.38	0.297.74e-03	0.17	0.15 (TC)	11,45,22,9	
80 ok L	0.0	1.8	0.01	0.95	2.61	1.76	1.78	2.61	0.32	0.09	0.42	0.14 (TC)	9,41,21,11
s=1,m=108	106.7	1.8	0.01	0.95	2.36	1.57	1.59	2.36	0.297.20e-03	0.17	0.14 (TC)	9,41,21,11	
93 NV L	0.0	1.8	0.08	0.75	2.58	1.51	1.53	1.53	0.40	1.44	0.06	0.03 (TC)	11,43,32,40
s=1,m=108	106.7	1.8	0.06	0.80	2.33	1.32	1.32	1.34	0.34	1.23	0.02	0.03 (TC)	11,43,45,40
94 NV L	0.0	1.8	0.05	0.83	2.87	1.68	1.68	1.68	0.41	1.53	0.03	0.02 (TC)	11,43,43,43
s=1,m=108	106.7	1.8	0.04	0.86	2.62	1.49	1.49	1.49	0.36	1.288.42e-03	0.02 (TC)	11,43,27,43	
95 NV L	0.0	1.8	0.07	0.78	3.07	1.82	1.83	1.82	0.46	1.36	0.05	0.03 (TC)	11,31,45,43
s=1,m=108	106.7	1.8	0.05	0.82	2.82	1.63	1.62	1.63	0.40	1.116.43e-03	0.03 (TC)	11,31,27,43	
96 NV L	0.0	1.8	0.94	0.0	0.0	1.88	1.86	1.86	0.0	2.63	0.07	0.04 (TC)	0,31,46,38
s=1,m=108	106.7	1.8	0.78	0.0	0.0	1.69	1.66	1.66	0.0	2.13	0.01	0.04 (TC)	0,31,38,38
97 NV L	0.0	1.8	0.17	0.58	2.96	1.80	2.69	2.38	0.60	1.09	0.10	0.04 (TC)	9,33,4,3
s=1,m=108	106.7	1.8	0.16	0.59	2.74	1.61	2.74	2.13	0.55	0.97	0.03	0.05 (TC)	11,33,11,3
98 ok L	0.0	1.8	0.02	0.93	2.02	1.33	1.84	1.84	0.25	0.10	0.17	0.11 (TC)	11,34,3,3
s=1,m=108	106.7	1.8	0.01	0.95	1.77	1.16	1.12	1.59	0.22	0.03	0.07	0.11 (TC)	11,32,26,3
99 NV L	0.0	1.8	0.02	0.93	1.76	1.21	1.22	1.45	0.22	0.06	1.45	0.22 (TC)	9,34,28,3
s=1,m=108	106.7	1.8	0.02	0.93	1.51	0.98	1.03	1.20	0.19	0.04	1.19	0.24 (TC)	9,33,24,3
110 NV L	0.0	1.8	0.03	0.91	1.73	1.14	1.20	1.42	0.22	0.07	1.49	0.22 (TC)	9,33,15,3
s=1,m=108	106.7	1.8	0.03	0.92	1.48	1.02	1.00	1.17	0.19	0.04	1.23	0.24 (TC)	9,34,15,3
111 ok L	0.0	1.8	0.04	0.87	1.48	1.08	1.08	1.08	0.20	0.10	0.05	0.02 (TC)	11,41,33,33
s=1,m=108	106.7	1.8	0.01	0.95	1.23	0.81	0.82	0.89	0.15	0.02	0.03	0.02 (TC)	11,34,21,33
112 NV L	0.0	1.8	0.16	0.61	2.36	1.36	1.42	1.41	0.46	1.24	0.05	0.03 (TC)	11,32,33,31
s=1,m=108	106.7	1.8	0.14	0.66	2.16	1.17	1.18	1.22	0.38	1.13	0.03	0.03 (TC)	9,32,20,31
113 NV L	0.0	1.8	1.25	0.0	0.0	1.42	1.97	1.42	0.0	3.01	0.04	0.02 (TC)	0,32,3,42
s=1,m=108	106.7	1.8	1.01	0.0	0.0	1.23	1.26	1.23	0.0	2.46	0.02	0.02 (TC)	0,32,21,42
114 ok L	0.0	1.8	0.07	0.77	2.23	1.34	1.34	1.77	0.34	0.487.70e-032.35e-03 (TC)		11,32,17,3	
s=1,m=108	106.7	1.8	0.06	0.80	1.98	1.15	1.15	1.52	0.29	0.436.24e-032.50e-03 (TC)		11,32,21,3	
115 ok L	0.0	1.8	0.06	0.79	2.22	1.34	1.33	2.22	0.33	0.474.47e-032.06e-03 (TC)		9,40,21,11	
s=1,m=108	106.7	1.8	0.05	0.84	1.97	1.15	1.13	1.97	0.27	0.387.43e-032.17e-03 (TC)		9,42,20,11	
116 ok L	0.0	1.8	0.07	0.77	2.20	1.33	1.32	1.33	0.33	0.488.09e-035.42e-04 (TC)		11,40,17,22	
s=1,m=108	106.7	1.8	0.06	0.81	1.95	1.14	1.13	1.13	0.28	0.44	0.015.75e-04 (TC)		11,40,17,22
124 NV L	0.0	1.8	0.17	0.56	0.99	0.72	0.75	0.75	0.21	0.38	1.26	0.18 (TC)	11,38,26,26
s=1,m=108	106.7	1.8	0.02	0.94	0.74	0.57	0.56	0.56	0.09	0.05	0.99	0.20 (TC)	11,37,26,26
125 ok L	0.0	1.8	0.01	0.96	1.16	0.76	0.78	0.78	0.14	0.04	0.72	0.10 (TC)	9,33,27,27
s=1,m=108	106.7	1.8	0.02	0.93	0.91	0.58	0.59	0.59	0.12	0.04	0.66	0.11 (TC)	9,31,27,27
126 ok L	0.0	1.8	0.02	0.93	1.14	0.76	0.77	0.77	0.14	0.06	0.74	0.10 (TC)	9,34,19,15
s=1,m=108	106.7	1.8	0.03	0.91	0.89	0.58	0.58	0.58	0.12	0.05	0.68	0.11 (TC)	9,32,19,15
127 NV L	0.0	1.8	0.03	0.90	1.05	0.74	0.78	0.78	0.14	0.10	1.13	0.16 (TC)	11,31,17,17
s=1,m=108	106.7	1.8	0.03	0.90	0.80	0.60	0.59	0.59	0.11	0.07	0.88	0.18 (TC)	11,34,17,17
128 ok L	0.0	1.8	0.01	0.95	0.53	0.34	0.34	0.34	0.07	0.01	0.74	0.09 (TC)	9,39,20,20
s=1,m=108	106.7	1.8	0.04	0.88	0.28	0.16	0.15	0.15	0.04	0.06	0.68	0.10 (TC)	9,46,19,20
129 ok L	0.0	1.8	0.01	0.94	0.52	0.33	0.33	0.33	0.06	0.02	0.76	0.08 (TC)	11,40,19,27
s=1,m=108	106.7	1.8	0.02	0.94	0.27	0.15	0.14	0.14	0.03	0.02	0.83	0.09 (TC)	11,41,20,27
130 ok L	0.0	1.8	0.01	0.95	0.70	0.50	0.49	0.49	0.09	0.02	0.02	0.03 (TC)	9,40,21,21
s=1,m=108	107.2	1.8	0.05	0.84	0.44	0.28	0.31	0.30	0.06	0.09	0.14	0.03 (TC)	9,20,22,21
131 NV L	0.0	1.8	0.01	0.95	1.05	0.72	0.72	1.05	0.13	0.01	1.45	0.25 (TC)	11,21,30,9
s=1,m=108	107.2	1.8	0.01	0.95	0.80	0.54	0.53	0.80	0.10	0.01	1.09	0.27 (TC)	11,40,30,9
132 NV L	0.0	1.8	0.02	0.92	1.06	0.72	0.72	1.06	0.14	0.03	1.47	0.25 (TC)	9,29,21,11
s=1,m=108	107.2	1.8	0.01	0.95	0.81	0.54	0.53	0.81	0.109.41e-03	1.09	0.27 (TC)	9,39,21,11	
133 ok L	0.0	0.4	0.03	0.90	0.24	0.14	0.14	0.14	0.03	0.07	0.34	0.05 (TC)	9,42,27,19
s=1,m=108	26.1	0.42.56e-03	0.99	0.18	0.09	0.09	0.09	0.09	0.022.62e-06	0.23	0.05 (TC)	9,27,27,19	
134 ok L	0.0	0.58.00e-03	0.97	0.28	0.16	0.15	0.15	0.15	0.03	0.02	0.36	0.06 (TC)	11,41,20,20
s=1,m=108	27.2	0.52.67e-03	0.99	0.21	0.10	0.10	0.10	0.10	0.031.34e-06	0.23	0.06 (TC)	9,22,20,20	
135 ok L	0.0	1.4	0.05	0.82	0.37	0.25	0.24	0.37	0.05	0.11	0.14	0.02 (TC)	9,40,22,11
s=1,m=108	86.1	1.49.97e-03	0.96	0.17	0.08	0.08	0.17	0.02	0.02	0.04	0.20	0.02 (TC)	9,39,21,11
136 ok L	0.0	1.4	0.01	0.95	0.77	0.51	0.51	0.51	0.09	0.02	0.92	0.13 (TC)	11,40,30,30
s=1,m=108	86.1	1.4	0.01	0.95	0.57	0.35	0.36	0.36	0.07	0.02	0.98	0.14 (TC)	11,40,19,30
137 ok L	0.0	1.4	0.01	0.96	0.76	0.52	0.51	0.51	0.099.82e-03	0.96	0.14 (TC)	9,39,21,21	
s=1,m=108	86.1	1.4	0.01	0.96	0.56	0.36	0.36	0.35	0.07	0.01	0.95	0.15 (TC)	9,39,20,21
138 ok L	0.0	1.1	0.04	0.87	0.43	0.32	0.32	0.32	0.06	0.11	0.89	0.10 (TC)	9,34,19,19
s=1,m=108	67.2	1.1	0.03	0.91	0.28	0.20	0.19	0.20	0.04	0.08	0.89	0.11 (TC)	9,34,21,19
139 ok L	0.0	1.8	0.06	0.82	2.57	1.47	1.47	1.47	0.37	0.93	0.015.87e-03 (TC)		11,43,45,29
s=1,m=108	107.2	1.8	0.03	0.88	2.32	1.28	1.27	1.27	0.31	0.647.82e-036.20e-03 (TC)		11,43,27,29	
140 NV L	0.0	1.8	0.04	0.87	2.66	1.52	1.51	1.51	0.36	1.058.34e-037.41e-03 (TC)		11,43,27,27	
s=1,m=108	107.2	1.8	0.02	0.91	2.41	1.33	1.31	1.32	0.31	0.70	0.017.81e-03 (TC)		11,45,28,27
141 ok L	0.0	1.8	0.05	0.83	2.81	1.61	1.60	1.61	0.40	0.956.49e-035.31e-03 (TC)		11,31,27,25	
s=1,m=108	107.2	1.8	0.03	0.89	2.56	1.42	1.42	1.41	0.34	0.61	0.015.58e-03 (TC)		11,35,29,25
142 NV L	0.0	1.8	0.80	0.0	0.0	1.64	1.61	1.61	0.0	2.04	0.015.47e-03 (TC)		0,31,38,34
s=1,m=108	107.2	1.8	0.44	0.34	2.61	1.45	1.43	1.42	0.90	1.137.35e-035.75e-03 (TC)		11,31,29,34	
143 ok L	0.0	1.8	0.16	0.60	2.86	1.65	2.86	2.53	0.56	0.85	0.03	0.03 (TC)	11,33,11,4
s=1,m=108	107.2	1.8	0.11	0.70	2.60	1.46	1.42	2.28	0.44	0.54	0.04	0.04 (TC)	11,33,24,4

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144	ok L	0.0	1.8	0.01	0.95	1.87	1.22	1.21	1.69	0.23	0.03	0.12	0.12 (TC)	11,32,25,3
	s=1,m=108	107.2	1.8	0.02	0.93	1.62	1.03	1.01	1.44	0.21	0.03	0.39	0.13 (TC)	11,32,25,3
145	ok L	0.0	1.8	0.02	0.93	1.66	1.12	1.15	1.15	0.21	0.04	0.99	0.14 (TC)	9,33,27,28
	s=1,m=108	107.2	1.8	0.02	0.94	1.41	0.95	0.95	0.96	0.18	0.02	0.89	0.15 (TC)	9,36,27,28
146	NV L	0.0	1.8	0.02	0.92	1.63	1.13	1.13	1.13	0.21	0.04	1.02	0.14 (TC)	9,34,15,19
	s=1,m=108	107.2	1.8	0.01	0.95	1.38	0.95	0.94	0.94	0.17	0.01	0.92	0.15 (TC)	9,32,19,19
147	ok L	0.0	1.8	0.01	0.95	1.28	0.96	0.95	0.84	0.16	0.02	0.02	0.05 (TC)	11,31,16,18
	s=1,m=108	107.2	1.8	0.03	0.89	1.03	0.69	0.67	0.64	0.14	0.06	0.19	0.06 (TC)	11,36,17,18
148	ok L	0.0	1.8	0.11	0.68	2.50	1.40	1.40	1.44	0.43	0.89	0.03	0.01 (TC)	11,32,20,33
	s=1,m=108	107.2	1.8	0.08	0.75	2.25	1.21	1.25	1.25	0.35	0.63	0.04	0.01 (TC)	11,32,33,33
149	NV L	0.0	1.8	0.94	0.0	0.0	1.33	1.34	1.82	0.0	2.20	0.02	0.03 (TC)	0,32,21,3
	s=1,m=108	107.2	1.8	0.51	0.34	2.05	1.14	1.18	1.57	0.71	1.28	0.03	0.03 (TC)	9,32,31,3
150	ok L	0.0	1.8	0.06	0.82	2.19	1.26	1.26	1.26	0.31	0.355.78e-034.44e-03	0.03	0.03 (TC)	11,32,21,21
	s=1,m=108	107.2	1.8	0.04	0.87	1.94	1.07	1.07	1.06	0.26	0.24	0.014.72e-03	0.03 (TC)	11,32,22,21
151	ok L	0.0	1.8	0.04	0.85	2.18	1.26	1.25	1.25	0.30	0.306.83e-034.49e-03	0.03	0.03 (TC)	9,42,20,21
	s=1,m=108	107.2	1.8	0.03	0.91	1.93	1.07	1.06	1.06	0.25	0.20	0.014.78e-03	0.03 (TC)	9,42,21,21
152	ok L	0.0	1.8	0.05	0.83	2.22	1.28	1.27	1.27	0.32	0.359.23e-033.85e-03	0.03	0.03 (TC)	11,40,17,21
	s=1,m=108	107.2	1.8	0.04	0.88	1.97	1.09	1.07	1.08	0.26	0.26	0.014.09e-03	0.03 (TC)	9,40,15,21
153	ok L	0.0	1.6	0.02	0.94	0.60	0.44	0.45	0.45	0.07	0.07	0.99	0.16 (TC)	11,37,25,26
	s=1,m=108	93.3	1.6	0.06	0.82	0.38	0.27	0.28	0.28	0.05	0.12	0.68	0.18 (TC)	11,37,25,26
154	ok L	0.0	0.5	0.01	0.96	0.88	0.56	0.57	0.57	0.11	0.04	0.64	0.07 (TC)	9,31,27,27
	s=1,m=108	27.2	0.5	0.02	0.95	0.82	0.51	0.53	0.53	0.10	0.06	0.61	0.08 (TC)	9,33,27,27
155	ok L	0.0	0.4	0.02	0.94	0.87	0.56	0.56	0.56	0.11	0.05	0.64	0.08 (TC)	9,32,19,19
	s=1,m=108	26.1	0.4	0.02	0.93	0.80	0.51	0.52	0.52	0.10	0.07	0.61	0.08 (TC)	9,34,19,19
156	ok L	0.0	1.6	0.04	0.88	0.63	0.46	0.46	0.46	0.08	0.09	0.90	0.15 (TC)	11,34,17,17
	s=1,m=108	93.3	1.6	0.05	0.84	0.41	0.30	0.29	0.29	0.06	0.10	0.61	0.17 (TC)	11,34,17,17
157	NV L	0.0	1.7	0.04	0.88	0.24	0.17	0.17	0.17	0.03	0.09	0.73	0.07 (TC)	9,34,21,21
	s=1,m=108	100.0	1.79.81e-03	0.966.81e-03	0.03.46e-042.71e-038.33e-04	0.0	0.96	0.04 (TC)	0.0	0.96	0.04 (TC)	0.0	0.04 (TC)	12,0,6,11
158	ok L	0.0	1.4	0.03	0.91	2.84	1.55	1.54	1.54	0.37	0.386.67e-039.41e-03	0.03	0.03 (TC)	11,43,27,27
	s=1,m=108	86.1	1.48.75e-03	0.96	2.64	1.40	1.38	1.38	1.38	0.32	0.07	0.029.80e-03	0.03 (TC)	11,43,30,27
159	ok L	0.0	1.4	0.02	0.93	2.77	1.52	1.50	1.50	0.35	0.44	0.017.80e-03	0.03 (TC)	11,45,28,28
	s=1,m=108	86.1	1.48.66e-03	0.96	2.57	1.33	1.34	1.34	1.34	0.31	0.08	0.018.14e-03	0.03 (TC)	11,46,28,28
160	ok L	0.0	1.4	0.03	0.91	2.84	1.56	1.56	1.56	0.37	0.41	0.018.10e-03	0.03 (TC)	11,31,29,29
	s=1,m=108	86.1	1.48.89e-03	0.96	2.64	1.40	1.40	1.40	1.40	0.32	0.07	0.018.44e-03	0.03 (TC)	11,35,29,29
161	NV L	0.0	1.4	0.39	0.33	2.51	1.59	1.57	1.57	0.90	0.936.81e-03	0.01 (TC)	0.01 (TC)	4,31,29,29
	s=1,m=108	86.1	1.4	0.02	0.95	2.69	1.43	1.42	1.42	0.33	0.05	0.02	0.01 (TC)	11,31,28,29
162	ok L	0.0	1.4	0.10	0.73	2.96	1.63	1.59	1.59	0.48	0.40	0.03	0.02 (TC)	11,37,24,28
	s=1,m=108	86.1	1.4	0.01	0.96	2.75	1.48	1.44	1.44	0.34	0.04	0.02	0.02 (TC)	11,37,24,28
163	ok L	0.0	1.4	0.02	0.93	1.60	0.98	0.99	1.42	0.20	0.03	0.41	0.13 (TC)	11,30,25,3
	s=1,m=108	86.1	1.4	0.04	0.88	1.40	0.92	0.82	1.22	0.19	0.15	0.31	0.13 (TC)	11,33,26,3
164	ok L	0.0	1.4	0.01	0.95	1.41	0.94	0.96	0.96	0.17	0.02	0.83	0.13 (TC)	9,36,27,28
	s=1,m=108	86.1	1.4	0.01	0.96	1.21	0.81	0.81	0.80	0.15	0.04	0.76	0.14 (TC)	9,33,27,28
165	ok L	0.0	1.4	0.01	0.96	1.39	0.97	0.95	0.95	0.17	0.01	0.86	0.13 (TC)	9,32,19,15
	s=1,m=108	86.1	1.4	0.02	0.94	1.19	0.81	0.79	0.79	0.15	0.05	0.79	0.14 (TC)	9,34,19,15
166	NV L	0.0	1.4	0.03	0.90	1.14	0.79	0.77	0.75	0.15	0.07	0.35	0.31 (TC)	11,32,17,18
	s=1,m=108	86.1	1.4	0.04	0.90	0.94	0.67	0.61	0.60	0.12	0.10	1.31	0.33 (TC)	11,31,17,18
167	ok L	0.0	1.4	0.07	0.80	2.75	1.51	1.48	1.47	0.40	0.44	0.03	0.02 (TC)	11,34,33,31
	s=1,m=108	86.1	1.49.17e-03	0.96	2.55	1.36	1.34	1.32	1.32	0.31	0.05	0.01	0.02 (TC)	9,34,17,31
168	NV L	0.0	1.4	0.42	0.38	2.53	1.37	1.39	1.39	0.79	0.99	0.036.84e-03	0.03 (TC)	11,32,31,15
	s=1,m=108	86.1	1.4	0.02	0.95	2.32	1.22	1.24	1.24	0.29	0.05	0.037.15e-03	0.03 (TC)	11,32,15,15
169	ok L	0.0	1.4	0.03	0.90	2.46	1.35	1.35	1.35	0.32	0.169.76e-033.69e-03	0.03	0.03 (TC)	11,32,22,22
	s=1,m=108	86.1	1.49.03e-03	0.96	2.26	1.19	1.18	1.19	1.19	0.28	0.02	0.013.87e-03	0.03 (TC)	11,32,17,22
170	ok L	0.0	1.4	0.02	0.93	2.45	1.35	1.33	1.34	0.31	0.13	0.015.16e-03	0.03 (TC)	9,42,21,22
	s=1,m=108	86.1	1.48.65e-03	0.96	2.25	1.20	1.18	1.19	1.19	0.27	0.02	0.015.41e-03	0.03 (TC)	9,42,21,22
171	ok L	0.0	1.4	0.03	0.91	2.57	1.41	1.39	1.39	0.33	0.168.07e-037.41e-03	0.03	0.03 (TC)	11,40,15,15
	s=1,m=108	86.1	1.48.74e-03	0.96	2.37	1.26	1.24	1.23	1.23	0.29	0.03	0.017.75e-03	0.03 (TC)	9,40,21,15
172	NV L	0.0	1.7	0.08	0.75	0.26	0.19	0.20	0.20	0.04	0.17	0.69	0.08 (TC)	11,37,25,25
	s=1,m=108	100.0	1.79.80e-03	0.96	0.03	0.02	0.01	0.023.16e-03	0.0	1.30	0.10	0.10 (TC)	0.10 (TC)	11,26,24,25
173	NV L	0.0	1.7	0.04	0.88	0.25	0.17	0.17	0.17	0.03	0.11	0.75	0.08 (TC)	9,33,29,29
	s=1,m=108	100.0	1.79.81e-03	0.96	0.016.73e-056.73e-058.81e-041.36e-034.57e-05	220.23	0.04 (TC)	0.04 (TC)	0.04 (TC)	0.04 (TC)	0.04 (TC)	0.04 (TC)	0.04 (TC)	9,36,36,4
174	ok L	0.0	1.7	0.07	0.77	0.27	0.20	0.20	0.20	0.04	0.14	0.64	0.08 (TC)	11,34,17,17
	s=1,m=108	100.0	1.79.80e-03	0.96	0.04	0.02	0.02	0.024.51e-03	0.0	0.86	0.09	0.09 (TC)	0.09 (TC)	11,35,16,17
175	ok L	0.0	1.1	0.03	0.90	0.44	0.32	0.33	0.33	0.06	0.09	0.89	0.10 (TC)	9,33,27,28
	s=1,m=108	66.1	1.1	0.03	0.91	0.29	0.20	0.20	0.21	0.04	0.09	0.91	0.11 (TC)	9,33,29,28
177	ok L	0.0	3.6	0.05	0.82	2.73	2.34	1.59	1.59	0.39	0.18	0.06	0.02 (TC)	4,36,17,17
	s=5,m=108	106.7	3.6	0.03	0.90	2.49	1.39	1.57	1.40	0.33	0.137.31e-03	0.02 (TC)	0.02 (TC)	11,33,31,17
178	ok L	0.0	3.6	0.24	0.43	1.30	0.79	0.57	0.81	0.35	0.64	0.11	0.02 (TC)	4,20,15,16
	s=5,m=108	106.7	3.6	0.04	0.87	1.30	0.37	0.37	0.62	0.17	0.53	0.04	0.02 (TC)	9,31,31,16
191	ok L	0.0	1.8	0.02	0.92	1.01	0.79	0.62	0.62	0.13	0.14	0.17	0.05 (TC)	9,45,44,44
	s=1,m=108	106.7	1.8	0.02	0.94	0.76	0.42	0.44	0.42	0.10	0.05	0.04	0.05 (TC)	9,44,46,44
192	ok L	0.0	1.8	0.02	0.94	0.74	0.47	0.54	0.52	0.09	0.07	0.067.35e-03	0.03 (TC)	11,44,45,29
	s=1,m=108	107.2	1.8	0.06	0.79	0.49	0.28	0.34	0.33	0.07	0.23	0.098.25e-03	0.03 (TC)	9,44,45,29
193	ok L	0.0	1.9	0.02	0.94	3.37	2.13	3.37	2.12	0.42	0.17	0.012.46e-03	0.03 (TC)	11,45,11,39
	s=1,m=108	113.3	1.9	0.04	0.86	3.11	1.92	3.11	1.92	0.42	0.59	0.022.56e-03	0.03 (TC)	11,39,11,39
194	ok L	0.0	1.9	0.01	0.95	4.04	2.52	4.04	2.50	0.50	0.17	0.02	0.01 (TC)	11,45,11,29
	s=1,m=108	113.3	1.9	0.03	0.90	3.78	2.32	3.78	2.29	0.49	0.62	0.03	0.01 (TC)	11,45,11,29
195	ok L	0.0	1.9	0.01	0.95	4.30	2.68	2.68	2.68	0.53	0.154.52e-035.31e-03	0.03	0.03 (TC)	11,33,29,29
	s=1,m=108	113.3	1.9	0.04	0.88	4.03	2.48	2.48	2.48	0.54	0.55	0.015.50e-03	0.03 (TC)	11,33,29,29
196	NV L	0.0	1.9	0.03	0.90	4.84	2.99	4.31	2.98	0.63	0.136.70e-038.38e-03	0.03	0.03 (TC)	11,32,3,28

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s=1,m=108	113.3	1.9	0.37	0.37	4.58	2.80	2.78	2.78	1.45	1.06	0.018.64e-03 (TC)	11,34,28,28
197 ok L	0.0	1.9	0.01	0.95	5.97	3.73	5.97	3.70	0.74	0.077.68e-03	0.03 (TC)	11,36,11,29
s=1,m=108	113.3	1.9	0.04	0.89	5.70	3.56	5.60	3.49	0.75	0.25	0.10 0.03 (TC)	11,37,4,29
198 ok L	0.0	1.9	0.01	0.94	3.17	2.13	3.17	3.17	0.39	0.03	0.08 0.02 (TC)	11,37,4,11
s=1,m=108	113.3	1.9	0.02	0.93	2.91	1.93	2.90	2.91	0.37	0.07	0.11 0.02 (TC)	11,33,4,11
199 NV L	0.0	1.9	0.01	0.95	4.24	2.85	2.87	4.15	0.538.85e-03	0.09	0.62 (TC)	4,38,29,3
s=1,m=108	113.3	1.9	0.02	0.94	3.98	2.72	3.98	3.88	0.49	0.08	1.44 0.64 (TC)	4,31,4,3
200 NV L	0.0	1.9	0.01	0.95	4.19	2.79	2.80	4.10	0.529.41e-03	0.09	0.62 (TC)	4,33,21,3
s=1,m=108	113.3	1.9	0.02	0.93	3.92	2.72	3.92	3.83	0.49	0.09	1.43 0.64 (TC)	4,32,4,3
201 ok L	0.0	1.9	0.02	0.94	2.93	1.96	2.04	2.20	0.37	0.029.78e-038.42e-03 (TC)		4,18,31,32
s=1,m=108	113.3	1.9	0.02	0.94	2.67	1.99	2.67	1.99	0.33	0.11	0.028.77e-03 (TC)	4,32,11,32
202 ok L	0.0	1.9	0.01	0.95	3.88	2.42	2.48	2.42	0.48	0.075.37e-039.43e-03 (TC)		11,32,31,20
s=1,m=108	113.3	1.9	0.05	0.85	3.62	2.22	2.21	2.21	0.50	0.31	0.029.79e-03 (TC)	11,32,20,20
203 NV L	0.0	1.9	0.06	0.86	3.10	2.06	2.03	1.98	0.42	0.27	0.016.13e-03 (TC)	11,31,21,20
s=1,m=108	113.3	1.9	0.53	0.35	2.14	1.85	2.46	1.77	0.72	1.13	0.026.41e-03 (TC)	12,45,3,20
204 ok L	0.0	1.9	0.08	0.74	2.62	1.65	1.68	1.65	0.42	0.687.30e-033.13e-04 (TC)		9,32,17,15
s=1,m=108	113.3	1.9	0.08	0.75	2.35	1.45	1.48	1.45	0.37	0.638.24e-033.29e-04 (TC)		11,32,17,15
205 ok L	0.0	1.9	0.09	0.71	2.59	1.63	1.66	1.65	0.43	0.774.81e-032.73e-04 (TC)		11,40,21,22
s=1,m=108	113.3	1.9	0.08	0.74	2.32	1.42	1.45	1.45	0.37	0.694.76e-032.87e-04 (TC)		9,40,17,22
206 ok L	0.0	1.9	0.09	0.72	2.49	1.61	1.60	2.49	0.41	0.666.25e-033.81e-04 (TC)		9,46,21,9
s=1,m=108	113.3	1.9	0.09	0.73	2.22	1.40	1.39	2.22	0.36	0.616.98e-034.00e-04 (TC)		9,40,21,9
207 ok L	0.0	1.9	0.02	0.93	1.60	1.12	1.07	1.25	0.20	0.029.72e-032.94e-03 (TC)		9,20,45,22
s=1,m=108	113.3	1.9	0.03	0.90	1.34	1.03	1.34	1.04	0.17	0.05	0.013.14e-03 (TC)	9,40,9,22
208 ok L	0.0	1.9	0.01	0.95	2.29	1.64	2.28	2.28	0.288.06e-03	0.10	0.16 (TC)	11,45,9,29
s=1,m=108	113.3	1.9	0.01	0.95	2.02	1.36	1.35	2.02	0.25	0.03	0.28 0.17 (TC)	11,40,22,9
209 ok L	0.0	1.9	0.01	0.95	2.28	1.54	1.54	2.28	0.287.31e-03	0.10	0.15 (TC)	9,41,21,11
s=1,m=108	113.3	1.9	0.01	0.95	2.02	1.46	1.34	2.02	0.25	0.02	0.28 0.16 (TC)	9,40,21,11
210 ok L	0.0	3.9	0.03	0.89	2.56	2.24	1.55	2.12	0.34	0.057.37e-034.57e-03 (TC)		11,32,31,20
s=5,m=108	113.3	3.9	0.08	0.73	2.29	1.91	2.03	1.91	0.37	0.20	0.024.77e-03 (TC)	4,34,32,20
211 NV L	0.0	3.9	0.05	0.86	1.27	0.30	0.30	0.30	0.17	0.20	0.049.80e-03 (TC)	9,31,31,31
s=5,m=108	113.3	3.9	0.57	0.29	1.01	0.10	0.10	0.10	0.40	3.00	0.09 0.01 (TC)	9,31,31,31
212 ok L	0.0	1.4	0.07	0.78	0.46	0.27	0.31	0.26	0.07	0.21	0.09 0.04 (TC)	9,44,45,42
s=1,m=108	86.1	1.4	0.02	0.95	0.25	0.11	0.11	0.11	0.03	0.17	0.43 0.05 (TC)	9,42,46,42
213 NV L	0.0	1.7	0.04	0.86	3.12	1.91	3.12	1.90	0.42	0.81	0.02 0.03 (TC)	11,43,11,40
s=1,m=108	100.0	1.7	0.07	0.77	2.88	1.73	1.72	1.72	0.44	1.27	0.06 0.03 (TC)	11,43,32,40
214 NV L	0.0	1.7	0.03	0.90	3.63	2.20	3.63	2.21	0.47	0.86	0.03 0.02 (TC)	11,45,11,30
s=1,m=108	100.0	1.7	0.05	0.85	3.39	2.02	2.02	2.03	0.47	1.32	0.02 0.02 (TC)	11,43,43,30
215 NV L	0.0	1.7	0.04	0.88	3.86	2.36	2.36	2.36	0.51	0.75	0.02 0.02 (TC)	11,31,29,43
s=1,m=108	100.0	1.7	0.06	0.81	3.63	2.18	2.18	2.18	0.53	1.18	0.04 0.02 (TC)	11,31,45,43
216 NV L	0.0	1.7	0.41	0.34	4.33	2.65	2.64	3.79	1.50	1.19	0.01 0.05 (TC)	11,34,28,3
s=1,m=108	100.0	1.7	0.69	0.0	0.0	2.47	3.56	3.56	0.0	1.92	0.08 0.05 (TC)	0,34,3,3
217 ok L	0.0	1.7	0.04	0.89	5.46	3.43	5.36	3.36	0.72	0.32	0.095.61e-03 (TC)	11,33,4,38
s=1,m=108	100.0	1.7	0.09	0.76	5.23	3.25	5.12	3.18	0.81	0.57	0.095.74e-03 (TC)	11,33,4,38
218 ok L	0.0	1.7	0.02	0.93	2.58	1.79	2.56	2.56	0.32	0.08	0.11 0.14 (TC)	11,37,4,4
s=1,m=108	100.0	1.7	0.02	0.94	2.35	1.54	1.55	2.33	0.29	0.09	0.15 0.15 (TC)	11,34,25,4
219 NV L	0.0	1.7	0.01	0.95	3.95	2.63	3.95	3.86	0.49	0.08	1.48 0.70 (TC)	4,31,4,3
s=1,m=108	100.0	1.7	0.01	0.96	3.72	2.45	3.72	3.62	0.46	0.06	2.77 0.72 (TC)	4,31,4,3
220 NV L	0.0	1.7	0.02	0.94	3.89	2.68	3.89	3.81	0.49	0.09	1.47 0.70 (TC)	4,32,4,3
s=1,m=108	100.0	1.7	0.01	0.95	3.66	2.50	3.66	3.57	0.45	0.06	2.74 0.72 (TC)	4,32,4,3
221 ok L	0.0	1.7	0.02	0.94	2.34	1.60	1.60	1.71	0.29	0.14	0.02 0.02 (TC)	4,32,32,33
s=1,m=108	100.0	1.7	0.03	0.90	2.11	1.53	1.51	1.53	0.28	0.09	0.04 0.02 (TC)	11,33,41,33
222 ok L	0.0	1.7	0.05	0.85	3.70	2.27	2.27	2.33	0.51	0.40	0.02 0.05 (TC)	11,32,20,21
s=1,m=108	100.0	1.7	0.08	0.77	3.47	2.09	2.15	2.15	0.53	0.62	0.07 0.05 (TC)	11,32,21,21
223 NV L	0.0	1.7	0.55	0.34	2.14	1.82	2.41	1.83	0.74	1.19	0.02 0.06 (TC)	12,41,3,33
s=1,m=108	100.0	1.7	0.94	0.0	0.0	1.55	1.65	1.65	0.0	2.06	0.12 0.06 (TC)	0,34,33,33
224 ok L	0.0	1.7	0.08	0.76	2.38	1.46	1.49	1.95	0.37	0.578.21e-031.29e-03 (TC)		11,32,17,3
s=1,m=108	100.0	1.7	0.07	0.77	2.15	1.28	1.31	1.71	0.33	0.557.87e-031.36e-03 (TC)		11,32,17,3
225 ok L	0.0	1.7	0.08	0.75	2.36	1.47	1.46	2.14	0.37	0.614.74e-038.41e-04 (TC)		9,40,21,4
s=1,m=108	100.0	1.7	0.07	0.79	2.13	1.29	1.28	1.91	0.32	0.534.60e-038.83e-04 (TC)		9,40,21,4
226 ok L	0.0	1.7	0.08	0.74	2.29	1.43	1.43	1.42	0.36	0.566.84e-034.53e-04 (TC)		11,40,21,20
s=1,m=108	100.0	1.7	0.07	0.76	2.06	1.25	1.25	1.24	0.32	0.538.46e-034.77e-04 (TC)		11,40,17,20
227 ok L	0.0	1.7	0.03	0.90	1.25	0.94	0.92	0.87	0.16	0.06	0.024.35e-03 (TC)	9,44,21,20
s=1,m=108	100.0	1.7	0.02	0.94	1.02	0.76	0.79	0.69	0.13	0.03	0.024.69e-03 (TC)	9,40,12,20
228 ok L	0.0	1.7	0.01	0.96	1.91	1.31	1.29	1.29	0.23	0.03	0.39 0.14 (TC)	11,40,22,30
s=1,m=108	100.0	1.7	0.02	0.94	1.68	1.15	1.11	1.11	0.21	0.03	0.76 0.14 (TC)	11,45,30,30
229 ok L	0.0	1.7	0.01	0.96	1.91	1.35	1.28	1.28	0.23	0.02	0.38 0.14 (TC)	9,40,21,21
s=1,m=108	100.0	1.7	0.02	0.93	1.67	1.17	1.10	1.10	0.21	0.03	0.76 0.15 (TC)	9,40,21,21
230 ok L	0.0	3.4	0.08	0.73	1.97	1.59	1.20	1.20	0.32	0.21	0.023.34e-03 (TC)	4,32,33,33
s=5,m=108	100.0	3.4	0.03	0.89	1.74	1.33	1.06	1.02	0.23	0.036.82e-033.54e-03 (TC)		11,42,31,33
231 NV L	0.0	3.4	0.55	0.33	0.78	0.20	0.20	0.67	0.27	1.54	0.18 0.04 (TC)	12,31,31,3
s=5,m=108	100.0	3.4	0.03	0.91	0.72	0.02	0.02	0.44	0.09	2.31	0.29 0.05 (TC)	9,31,31,3
232 ok L	0.0	3.6	0.05	0.84	1.00	0.60	0.68	0.60	0.14	0.168.72e-034.34e-03 (TC)		11,37,18,33
s=5,m=108	106.7	3.6	0.03	0.88	0.75	0.41	0.41	0.41	0.10	0.07	0.034.82e-03 (TC)	11,33,33,33
233 NV L	0.0	3.6	0.04	0.91	0.508.52e-038.52e-03		0.33	0.06	7.13	10.83	0.05 (TC)	9,39,39,3
s=5,m=108	106.7	3.6	0.50	0.60	0.25	0.07	0.06	0.09	0.05	0.66	1.70 0.07 (TC)	9,20,7,3
234 ok L	0.0	3.6	0.04	0.88	0.60	0.36	0.43	0.40	0.08	0.13	0.039.38e-03 (TC)	11,36,16,17
s=5,m=108	107.2	3.6	0.12	0.67	0.34	0.17	0.18	0.21	0.06	0.40	0.09 0.01 (TC)	11,34,18,17
235 ok L	0.0	3.6	0.06	0.78	0.66	0.56	0.30	0.64	0.10	0.14	0.05 0.03 (TC)	4,32,31,3
s=5,m=108	107.2	3.6	0.16	0.58	0.41	0.10	0.10	0.39	0.08	0.34	0.15 0.04 (TC)	4,31,31,3

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236	NV L	0.0	2.9	0.16	0.60	0.21	0.12	0.13	0.13	0.04	0.45	0.37	0.06 (TC)	11,31,20,16	
	s=5,m=108	86.1	2.9	0.28	0.37	6.93e-03		0.06	9.3e-03	9.07e-03	2.20e-03	0.0	0.99	0.02 (TC)	9,0,9,11
237	NV L	0.0	2.9	0.27	0.39	0.26	0.19	0.14	0.25	0.08	0.58	0.09	8.52e-03 (TC)	4,42,33,3	
	s=5,m=108	86.1	2.9	0.50	0.72	0.06	6.69e-05	6.69e-05	0.04	9.40e-03	119.64	36.43	0.01 (TC)	11,17,17,3	
241	ok L	0.0	1.8	0.03	0.90	2.17	1.50	1.64	1.64	0.28	0.15	0.08	0.04 (TC)	11,41,26,26	
	s=1,m=108	106.7	1.8	0.01	0.95	1.92	1.39	1.27	1.45	0.24	0.01	0.03	0.04 (TC)	11,40,43,26	
242	ok L	0.0	1.9	0.01	0.95	1.80	1.29	1.32	1.80	0.22	0.01	0.02	5.28e-03 (TC)	11,43,45,11	
	s=1,m=108	113.3	1.9	0.02	0.94	1.53	1.09	1.53	1.50	0.19	0.03	0.03	5.65e-03 (TC)	11,43,11,4	
243	ok L	0.0	1.7	0.02	0.94	1.44	1.08	0.93	0.91	0.18	0.03	0.04	0.04 (TC)	11,43,46,44	
	s=1,m=108	100.0	1.7	0.02	0.93	1.21	0.92	0.73	0.73	0.15	0.12	0.15	0.04 (TC)	11,45,44,44	

Elem.	h0/t	Ecc/t(M)	Fi t	P/Ao	P/Ao(s)	P/Ap	Ver Mo	Ver Mo(S)	Ver Mp	Ver. V
	7.16	1.25	0.0	6.24	4.02	6.24	1.50	119.64	220.23	0.86

Suzzara, 10/12/2021

Il tecnico

Dott. Ing. Claudio Vincenzi